



# Analyses of Hydrogen Storage Materials and On-Board Systems

Project ID #  
st\_12\_lasher

Compressed and Liquid Hydrogen  
Carrier System Cost Assessments

DOE Merit Review  
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Reference: D0268

## Timeline

- ◆ Start date: June 2004
- ◆ End date: June 2009
- ◆ 80% Complete

## Budget

- ◆ Total project funding
  - DOE share = \$1.5M
  - No cost share
- ◆ FY08 = \$350k
- ◆ FY09 = \$261k (plan)

## Barriers

- ◆ A. System Weight and Volume
- ◆ B. System Cost
- ◆ K. System Life Cycle Assessments

## Collaboration

- ◆ Design and performance assessment: Argonne and other National Labs
- ◆ Technical input: Centers of Excellence and other developers
- ◆ Review: Tech Teams and other stakeholders

**This project provides an independent cost assessment of the hydrogen storage technologies being developed for the DOE Grand Challenge.**

Objective	Description
<b>Overall</b>	Help guide DOE and developers toward promising R&D and commercialization pathways by evaluating the status of the various on-board hydrogen storage technologies on a consistent basis
<b>On-Board Storage System Assessment</b>	Evaluate or develop system-level designs for the on-board storage system to project: 1) Bottom-up factory cost 2) Weight and volume (ANL lead)
<b>Off-Board Fuel Cycle Assessment</b>	Evaluate or develop designs and cost inputs for the fuel cycle to project: 1) Refueling cost 2) Well-to-Tank energy use and GHG emissions (ANL lead)

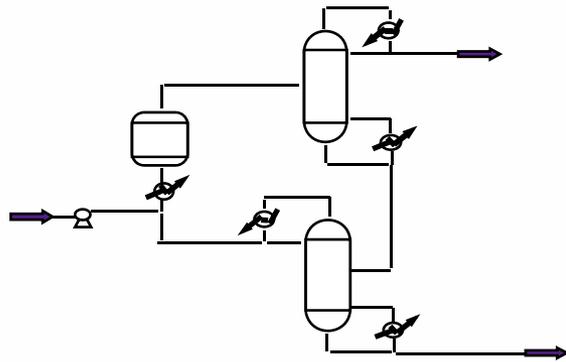
**Last year’s objective was to evaluate a liquid hydrogen carrier (LCH<sub>2</sub>) and update our compressed hydrogen storage assessments.**



The on-board cost and performance assessments are based on detailed technology assessment and bottom-up cost modeling.

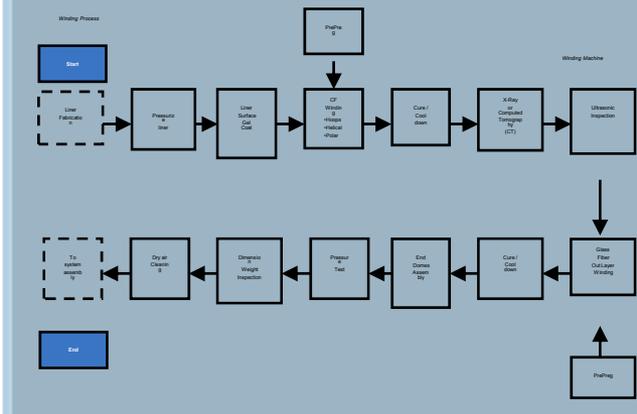
**Technology Assessment**

- Perform Literature Search
- Outline Assumptions
- Develop System Requirements and Design Assumptions
- Obtain Developer Input



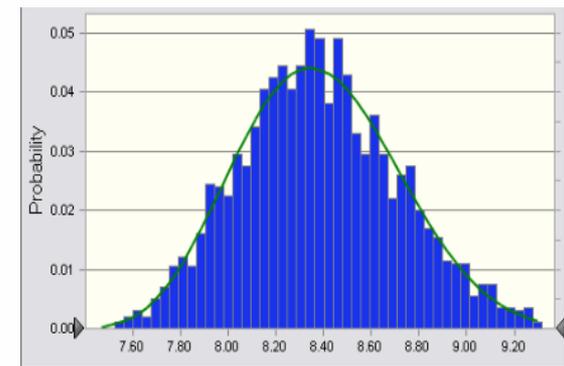
**Cost Model and Estimates**

- Develop BOM
- Specify Manufacturing Processes and Equipment
- Determine Material and Processing Costs
- Develop Bulk Cost Assumptions



**Overall Model Refinement**

- Obtain Developer and Industry Feedback
- Revise Assumptions and Model Inputs
- Perform Sensitivity Analyses (single and multi-variable)

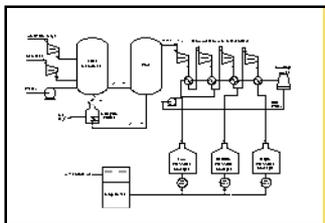


BOM = Bill of Materials



The off-board assessment makes use of existing models to calculate cost and performance for each technology on a consistent basis.

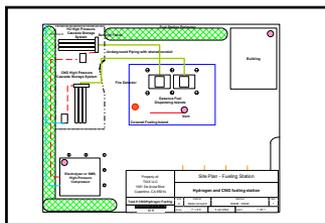
### Conceptual Design



- ◆ System layout and requirements

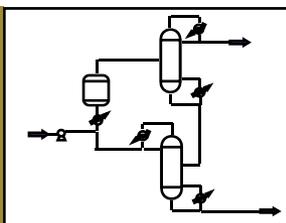


### Site Plans



- ◆ Safety equipment, site prep, labor and land costs

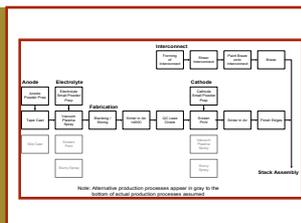
### Process Simulation



- ◆ Energy requirements
- ◆ Equipment size/specs

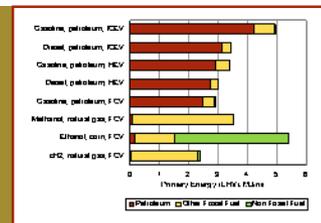


### Capital Cost Estimates



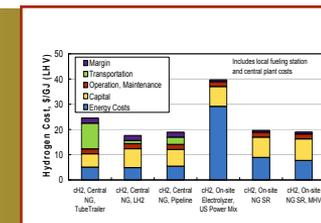
- ◆ High and low volume equipment costs

### ANL/GREET Model



- ◆ WTT energy use
- ◆ WTT GHG

### TIAX/H2A Model



- ◆ Equivalent hydrogen selling price



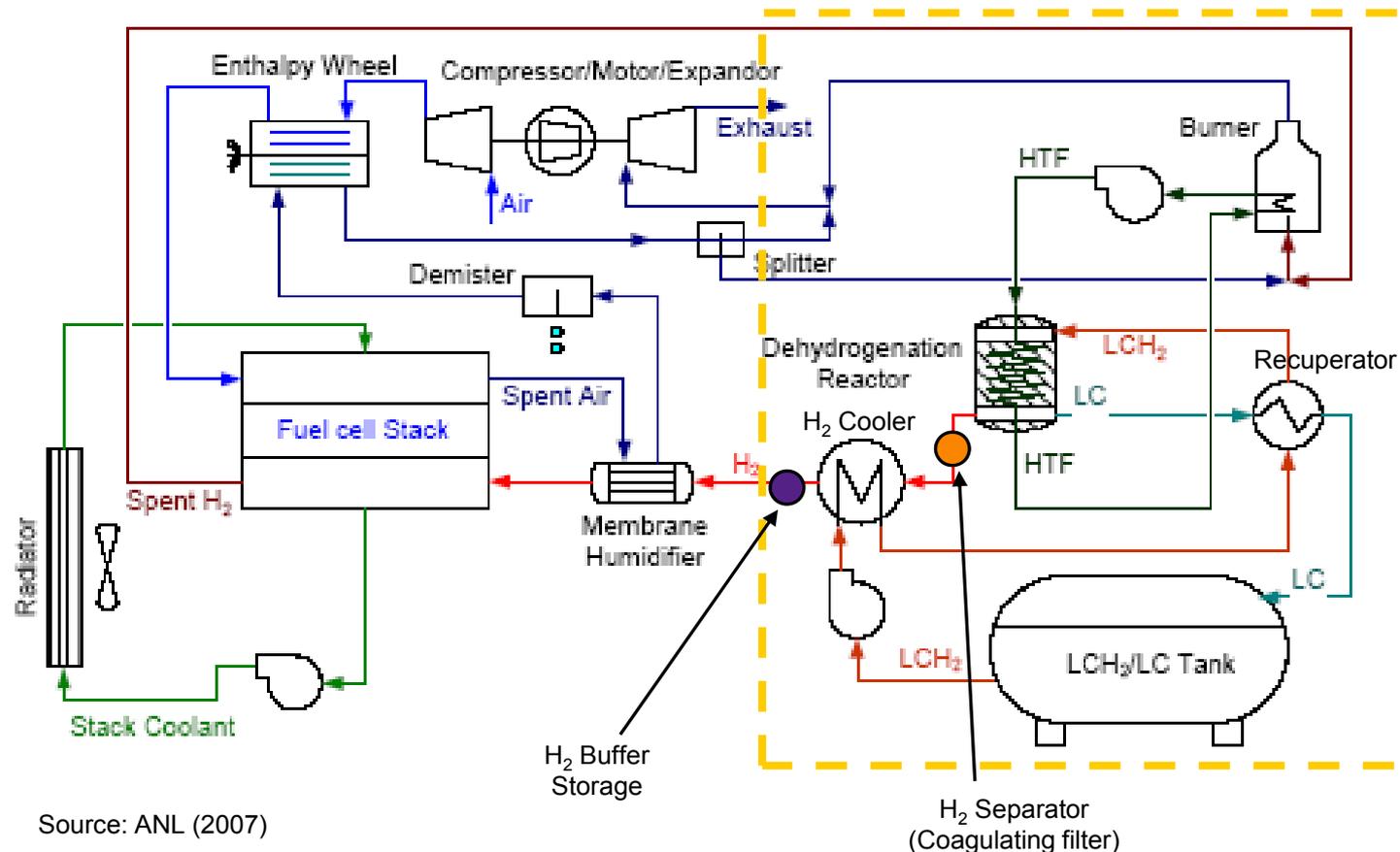
## We completed on-board and off-board assessments of LCH<sub>2</sub> and updated our compressed H<sub>2</sub> assessment since the last Review.

- ◆ Completed liquid hydrogen carrier (LCH<sub>2</sub>) system cost assessments
  - Based on ANL's performance assessment of Air Products and Chemicals Inc. (APCI) regenerable organic liquid carrier (n-ethylcarbazole-like material<sup>1</sup>)
  - High-volume (500,000 units/yr) on-board system factory cost projection = \$15.4/kWh useable H<sub>2</sub>
  - On-board system weight estimate = 2.2 wt.%; volume estimate = 19 g H<sub>2</sub>/L
  - Mature market (i.e., 250 TPD H<sub>2</sub> eq.) refueling cost projection = \$4.74/kg H<sub>2</sub> eq.
- ◆ Updated 5 and 10-ksi compressed hydrogen on-board system factory cost assessment
  - Made slight adjustments to the tank safety factor and carbon fiber requirements to be consistent with ANL's updated analysis assumptions and results
  - Applied tank safety factor to nominal pressure (i.e., 5 and 10 ksi) rather than max filling over pressure (i.e., 6.25 and 12.5 ksi)
  - High-volume projection = \$15.6 and \$23/kWh useable H<sub>2</sub> for 5 and 10-ksi, respectively
  - On-board system weight estimates = 5.9 and 4.6 wt.%; volume estimates = 18 and 25 g H<sub>2</sub>/L for 5 and 10-ksi, respectively
- ◆ Completed review of Rohm & Haas (R&H)'s Ammonia Borate (AB) regen. and 1<sup>st</sup> fill cost projections
  - Based on R&H plant configuration and performance assessments
  - Mature market (i.e., 100 TPD H<sub>2</sub> eq.) AB regeneration cost projection = \$8/kg H<sub>2</sub> eq.
  - Mature market (i.e., 10,000 TPY AB) AB 1<sup>st</sup> fill cost projection = \$9/kg AB

<sup>1</sup> N-ethylcarbazole is toxic and has a low weight % making it relatively inappropriate for an actual on-board storage medium, however it is being used as a representative material for expected carriers to be developed and allows analysis regarding the system, and delivery to be completed.

We used the on-board system definition and design developed by APCI<sup>1</sup> and ANL<sup>2</sup> as the basis of our LCH<sub>2</sub> factory cost assessment.

On-Board Storage System to be Evaluated (yellow dashed box)



Source: ANL (2007)

<sup>1</sup> "Hydrogen Storage by Reversible Hydrogenation of Liquid-Phase Hydrogen Carriers", Cooper, A. and Pez, G., 2007 DOE H<sub>2</sub> Program Review

<sup>2</sup> "System Level Analysis of Hydrogen Storage Options", Ahluwalia, R.K. et al., 2007 DOE H<sub>2</sub> Program Review, May 2007

**Media and storage tank assumptions and specifications were based on previous TIAX analyses and discussions with APCI and ANL<sup>1,2</sup>.**

System Element	Design Parameter	Value	Basis/Comment
<b>Media/System</b>	Media/material (prototypical)	N-ethylcarbazole <sup>3</sup>	ANL <sup>2</sup> , APCI <sup>1</sup>
	Material H <sub>2</sub> storage capacity	5.8 wt% <sup>3</sup>	ANL <sup>2</sup> , APCI <sup>1</sup>
	Storage system efficiency	67.7%	ANL <sup>2</sup> ; includes H <sub>2</sub> utilized to fire burner only (does not include 95% reactor conversion efficiency)
	LCH <sub>2</sub> solution density	1200 kg/m <sup>3</sup>	ANL <sup>2</sup>
	LC solution density	950 kg/m <sup>3</sup>	ANL <sup>2</sup>
<b>LCH<sub>2</sub>/LC Storage Tank</b>	Usable H <sub>2</sub> capacity	5.6 kg	Design basis; note: ANL <sup>2</sup> analysis done for 6.4 kg usable H <sub>2</sub>
	Stored H <sub>2</sub> capacity	8.7 kg	Calculated based on 95% conversion efficiency and 67.7% storage efficiency; note: ANL <sup>2</sup> analysis done for 10 kg stored H <sub>2</sub>
	Tank material of construction	HDPE	ANL <sup>2</sup>
	% excess tank volume	10%	Over fuel volume, to account for sloshing
	Bladder/separator?	Yes	Single tank design; needed to separate LCH <sub>2</sub> from LC
	Temperature	70 °C	Needed to prevent solidification

<sup>1</sup> "Hydrogen Storage by Reversible Hydrogenation of Liquid-Phase Hydrogen Carriers", Cooper, A. and Pez, G., 2007 DOE Hydrogen Program Review

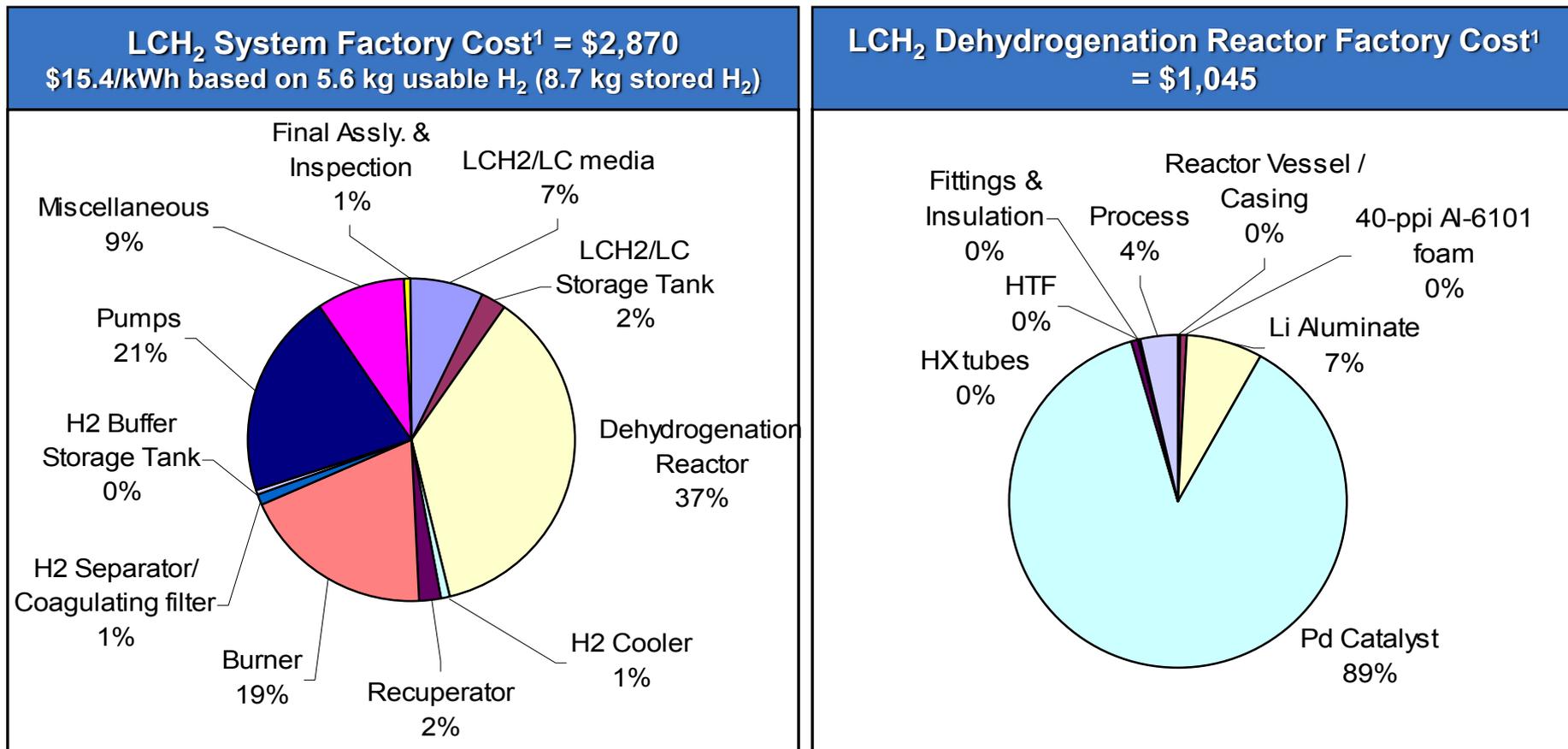
<sup>2</sup> "System Level Analysis of Hydrogen Storage Options", Ahluwalia, R.K. et al., 2007 DOE Hydrogen Program Review, May 2007

<sup>3</sup> N-ethylcarbazole is toxic and has a low weight % making it relatively inappropriate for an actual on-board storage medium, however it is being used as a representative material for expected carriers to be developed and allows analysis regarding the system, and delivery to be completed.

**Other component design assumptions are presented in the Appendix.**



**We estimate the high-volume factory cost<sup>1</sup> of the system to be about \$15.4/kWh, of which ~32% is due to the cost of the Pd catalyst.**



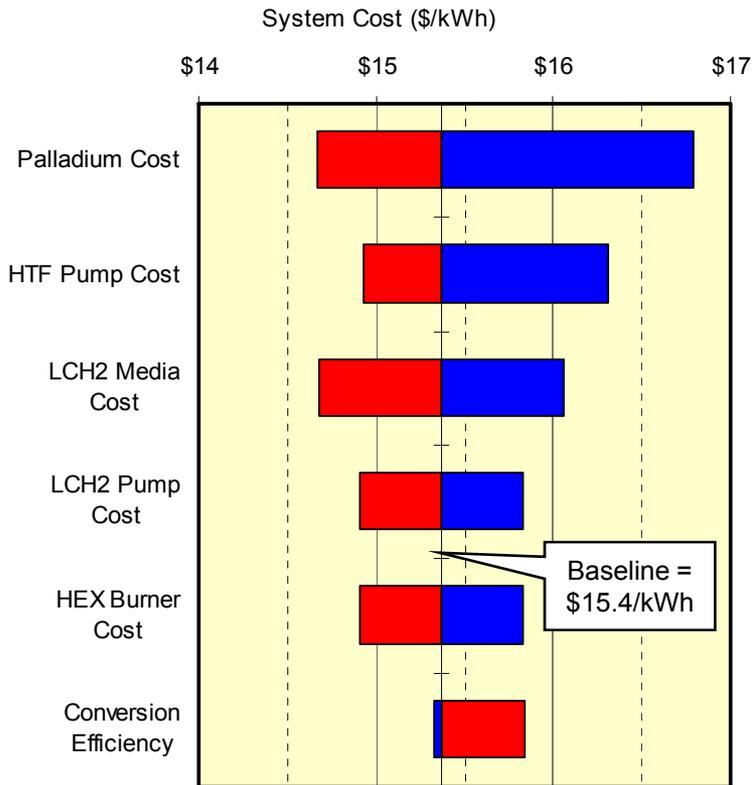
Note: A trade-off study was not performed on the size/cost of the pumps versus size/cost of the reactor sub-system and burner.

<sup>1</sup> Cost includes deflation by 9.27% to Year 2005 USD.

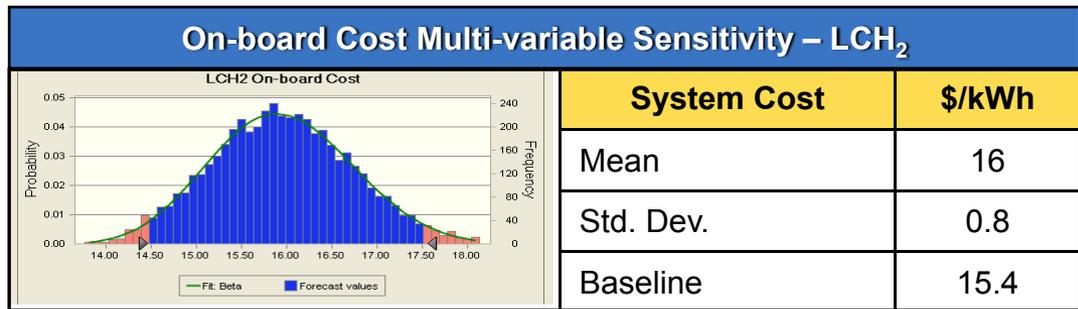


# Uncertainty in the catalyst, carrier media, and purchased component prices significantly affect the projected cost of the liquid carrier system.

**On-board Cost Sensitivity – Liquid Hydrogen Carrier (5.6 kg H<sub>2</sub>), \$/kWh**



Key Sensitivity Parameters	On-board Cost Sensitivity – LCH <sub>2</sub>			
	Base-line	Min	Max	Basis/Comment
Conversion Efficiency	95%	65%	100%	◆ Baseline from ANL 2007 DOE AMR <sup>1</sup> , min from APCI 2008 DOE AMR <sup>2</sup>
Palladium Cost (\$/troy oz.)	436	360	580	◆ Baseline from metalprices.com average ◆ Min and Max estimates from min and max LME values over the past year
HTF Pump Cost	\$400	\$300	\$600	◆ Baseline from catalog prices discounted by ~60%
LCH <sub>2</sub> Media Cost (per gal)	\$7	\$2	\$12	◆ Discussion with APCI
LCH <sub>2</sub> Pump Cost	\$200	\$100	\$300	◆ Baseline from catalog prices discounted by ~60%
HEX Burner Cost	\$400	\$300	\$500	◆ Baseline from catalog prices for natural gas burners discounted by ~60%.



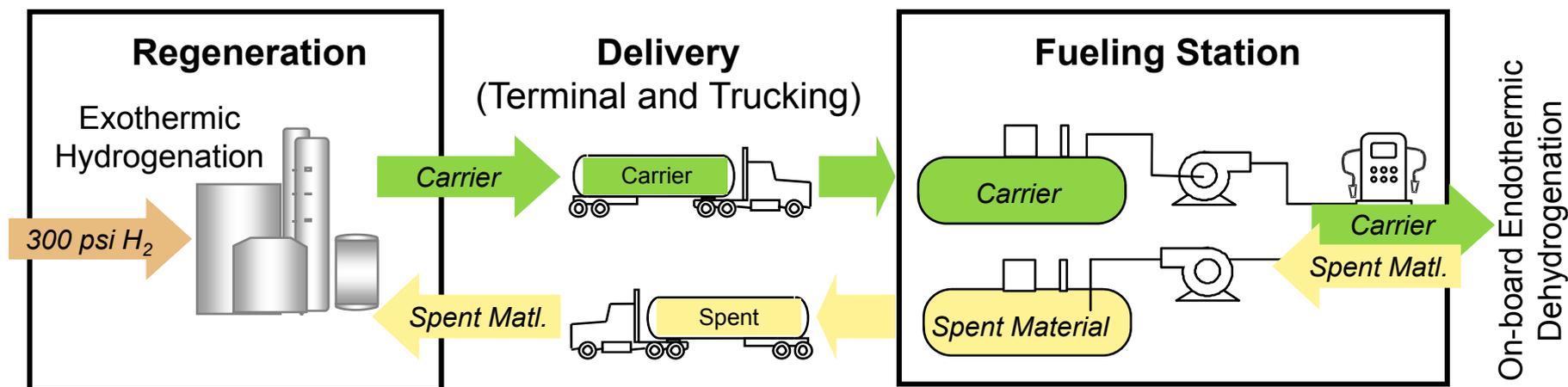
<sup>1</sup> "System Level Analysis of Hydrogen Storage Options", Ahluwalia, R.K. et al., 2007 DOE Hydrogen Program Review, May 2007

<sup>2</sup> "Reversible Liquid Carriers for an Integrated Production, Storage and Delivery of Hydrogen", Toseland, B. and Pez, G., 2008 DOE H<sub>2</sub> Program Review



## An H2A Carrier model was developed to evaluate the off-board refueling cost for LCH<sub>2</sub> and allow for direct comparison to other H<sub>2</sub> options.

- ◆ Most financial assumptions are maintained from the original H2A Delivery Components Model
- ◆ New calculation tabs were added as part of the DOE Delivery Project for novel carriers, resulting in the H2A Delivery Components Carrier Model v34
- ◆ These new calculation tabs were populated with inputs based on industry and developer feedback specifically for LCH<sub>2</sub> and SBH



The off-board assessment for novel carriers requires evaluation of regeneration, delivery and forecourt technologies.

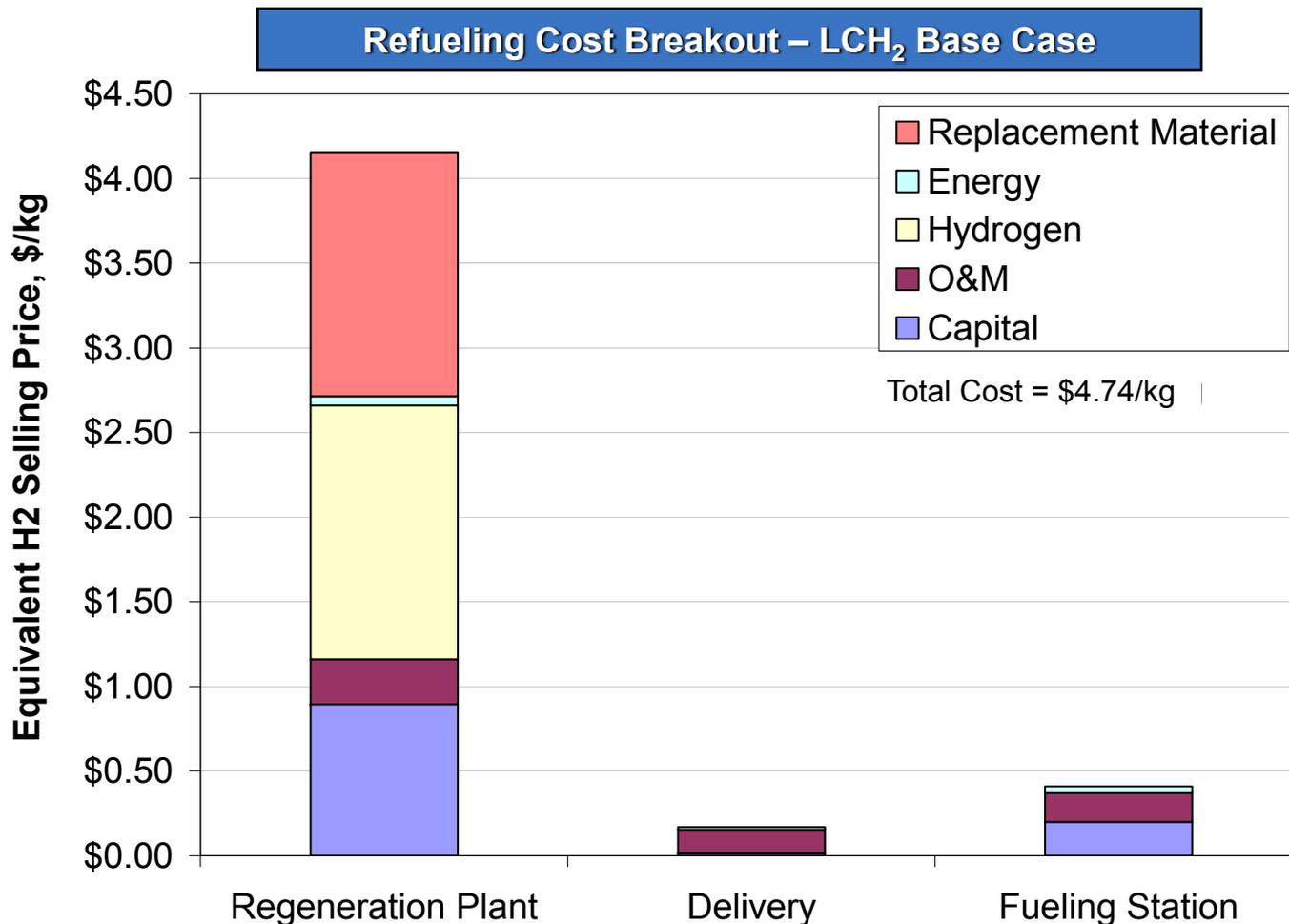
## The LCH<sub>2</sub> regeneration facility assumptions were based on previous H2A assessments and discussions and information provided by APCI.

Regeneration Plant Component	Assumptions
<b>Hydrogen</b>	Hydrogen is purchased as a pure gas at 20 bar for \$1.50/kg No losses are assumed
<b>Material Storage Tanks</b>	Storage for a 10-day plant shutdown and a 120-day summer peak period (10% above average demand) is included for hydrogenated material Equal amount of storage included for dehydrogenated material Two quarantine tanks are included for substandard material (five days of material) Assumed cost: \$0.42/gal (based on similar tanks in H2A)
<b>Carrier Material</b>	N-ethylcarbazole is estimated to cost between \$2-12/gal; \$7/gal used for baseline (industry estimate) Material replacement is estimated to fall between 0.5-5.0% of plant throughput; 2.75% used for baseline (APCI est.) Material allocation equals that required to fill all hydrogenated storage tanks
<b>Capital Cost</b>	Includes: compressors, reactors, tankage, distillation, heat exchangers, fluid power equipment, and power and instrumentation (combination of H2A and industry cost estimates) Range of 50-150% of estimated equipment capital cost used for sensitivity analysis
<b>Catalyst Loading and Replacement</b>	Assumed initial catalyst cost is \$170/kg and cost for replacement catalyst is \$155/kg (industry est.) Catalyst lifetime based on material processed: 350,000-1,000,000 kg <sub>m</sub> /kg <sub>c</sub> ; 500,000 baseline (industry est.)

**Delivery and Fueling Station design assumptions are presented in the Appendix.**



**Off-board cost results indicate that the major non-H<sub>2</sub> costs include capital costs at the regeneration plant and carrier material replacement.**



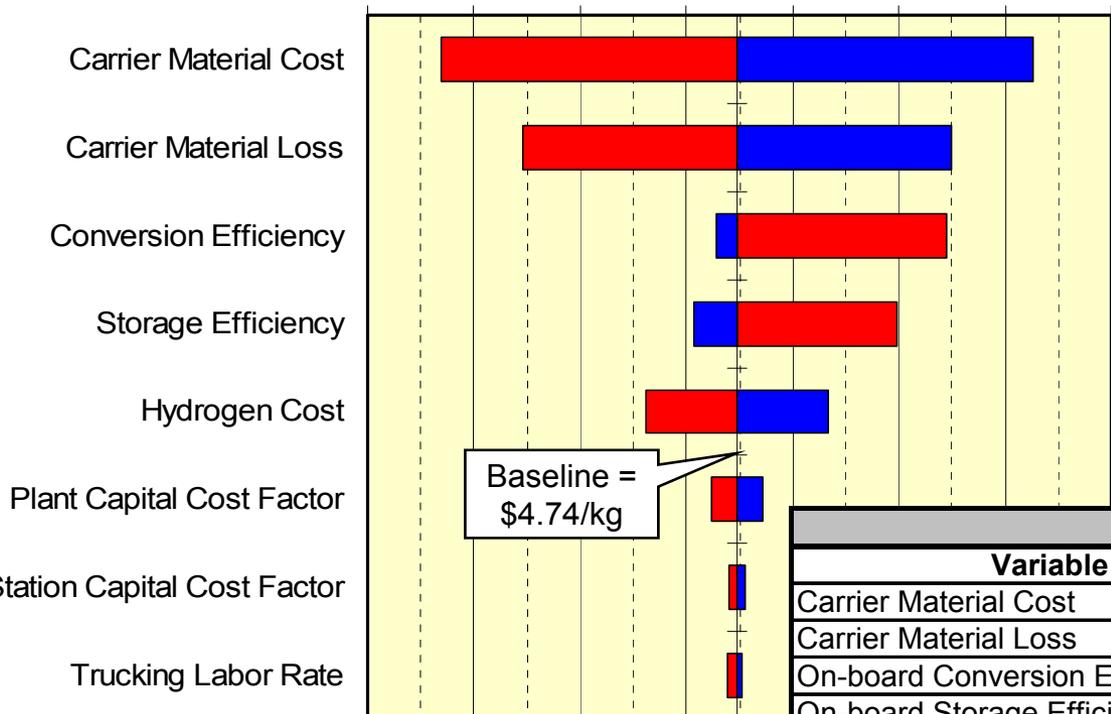
Note: Detailed assumptions are presented in the Appendix. If the carrier is used as an off-board transportation media only (i.e., fueling station dehydrogenation), the H<sub>2</sub> selling price would increase to about \$5.90/kg.



# Factors effecting the initial and replacement costs of carrier material have the greatest affect on the hydrogen selling price sensitivity.

## Refueling Cost Sensitivity - LCH<sub>2</sub>

Equivalent H2 Selling Price, \$/kg  
 \$3.0 \$3.5 \$4.0 \$4.5 \$5.0 \$5.5 \$6.0 \$6.5



		Values		
Variable	Units	Min	Baseline	Max
Carrier Material Cost	\$/gal	\$2	\$7	\$12
Carrier Material Loss	%	0.5%	2.75%	5%
On-board Conversion Efficiency	%	65%	95%	100%
On-board Storage Efficiency	%	50%	67.7%	75%
Hydrogen Cost	\$/kg	\$1	\$1.5	\$2
Plant Capital Cost Factor	%	50%	100%	150%
Fueling Station Capital Cost Factor	%	50%	100%	150%
Trucking Labor Rate	\$/hr	\$25	\$40	\$50



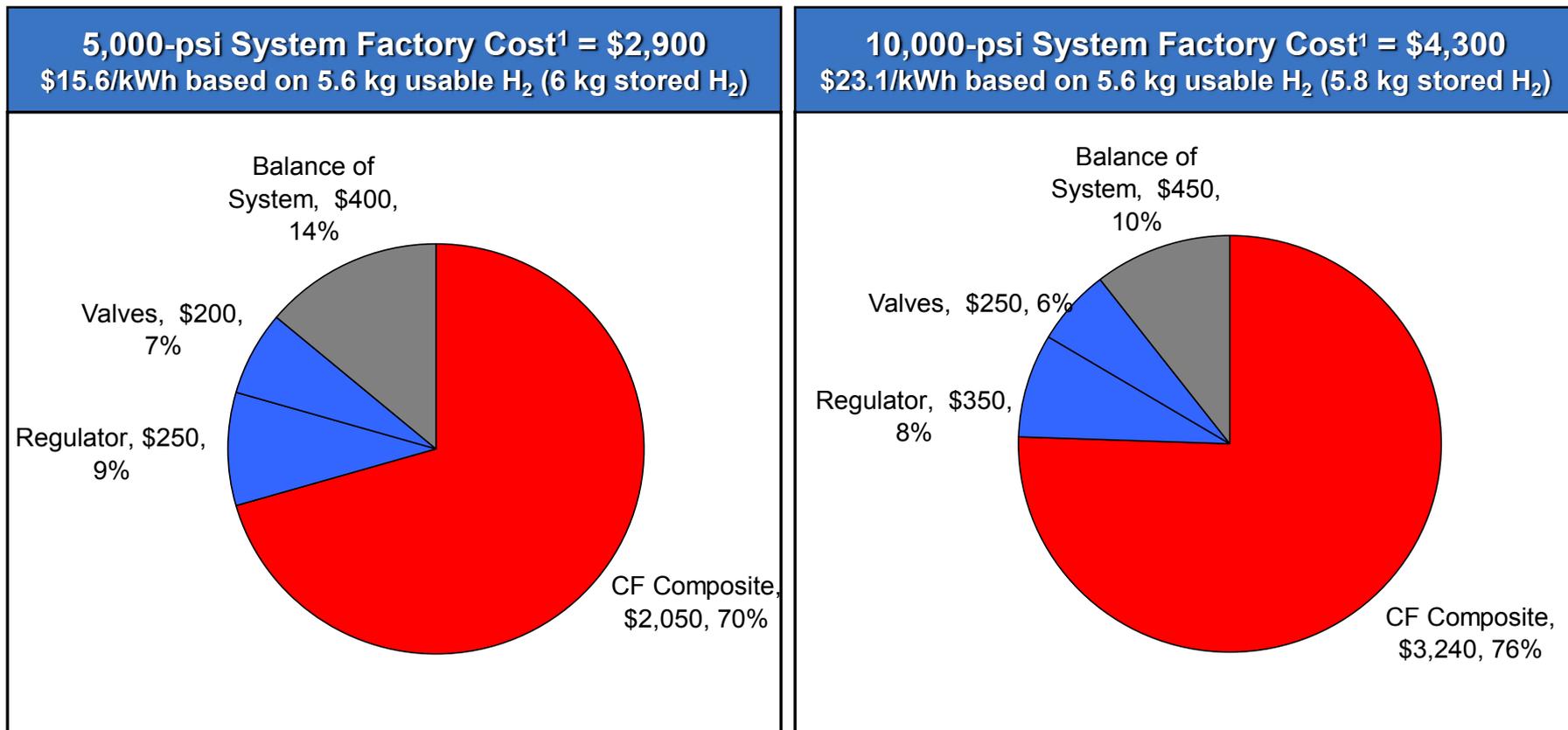
## We reviewed and updated our previous compressed tank design assumptions with DOE, Quantum, SCI, Toray and ANL.

Design Parameter	Base Case Value	Basis/Comment
Usable H <sub>2</sub> storage capacity	5.6 kg	Design assumption based on ANL drive-cycle modeling for 350 mile range assuming a mid-sized, hydrogen fuel cell vehicle
Tank size (water capacity)	261 L (5-ksi) 150 L (10-ksi)	Required for 5.6 kg useable H <sub>2</sub> capacity (6.0 and 5.8 kg total H <sub>2</sub> capacity for 5-ksi and 10-ksi tanks, respectively)
Carbon fiber type	Toray T700S	Consistent with industry use and other H <sub>2</sub> storage analyses
Safety factor	2.35	EIHP Rev 12b design criteria applied to nominal storage pressure (i.e., 5 ksi and 10 ksi)
Composite tensile strength	2,550 MPa	Toray material data sheet for 60% fiber by volume
Translation strength factors	82.5% (5-ksi) 63% (10-ksi)	Quantum, 2004
L/D Ratio	3	Discussions with Quantum, 2008; based on the outside of the CF wrapped tank
“Empty” pressure	290 psi	Discussions with Quantum, 2008
Max filling over pressure	25% design pressure	Required for fast fills to prevent under-filling
Tank liner	5 mm HDPE	Discussions with Quantum, 2008; typical for Type IV tanks
Overwrap	1 mm glass fiber	Discussions with Quantum, 2008, common but not functionally required
Protective end caps	10 mm foam	Discussions with Quantum, 2008

 = updated design parameter in 2008/2009



**Updated results show carbon fiber (CF) composite accounts for ~70% and 75% of the base case 5-ksi and 10-ksi system costs, respectively.**

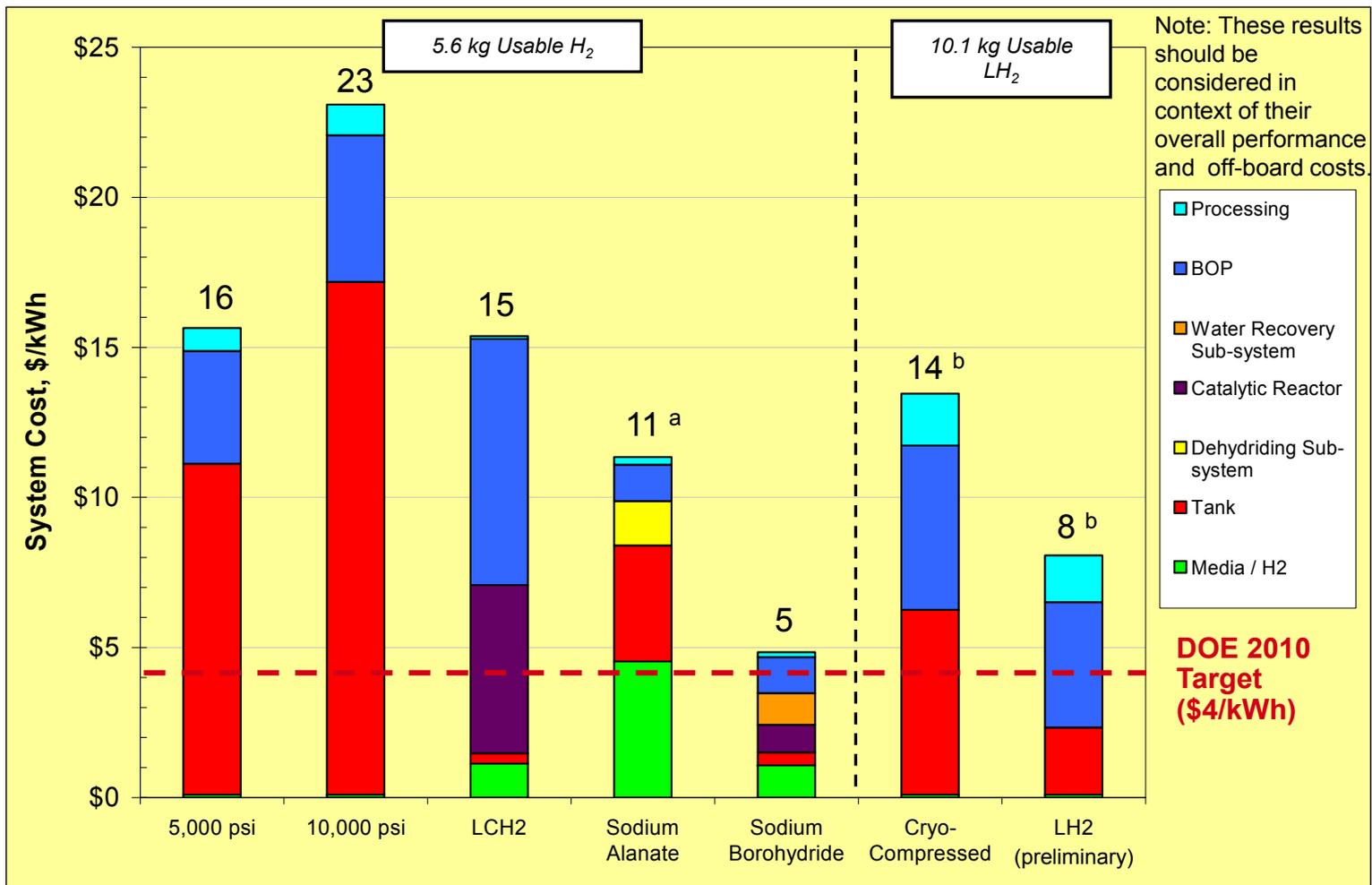


<sup>1</sup> Cost estimate in 2005 USD. Includes processing costs.

**Processing costs account for approximately 5% of the total cost, and are included above. Sensitivity results are presented in the Appendix.**



**5-ksi, 10-ksi, and LCH<sub>2</sub> on-board storage system costs are projected to be 4 - 6 times higher than the 2010 target, using base case assumptions.**

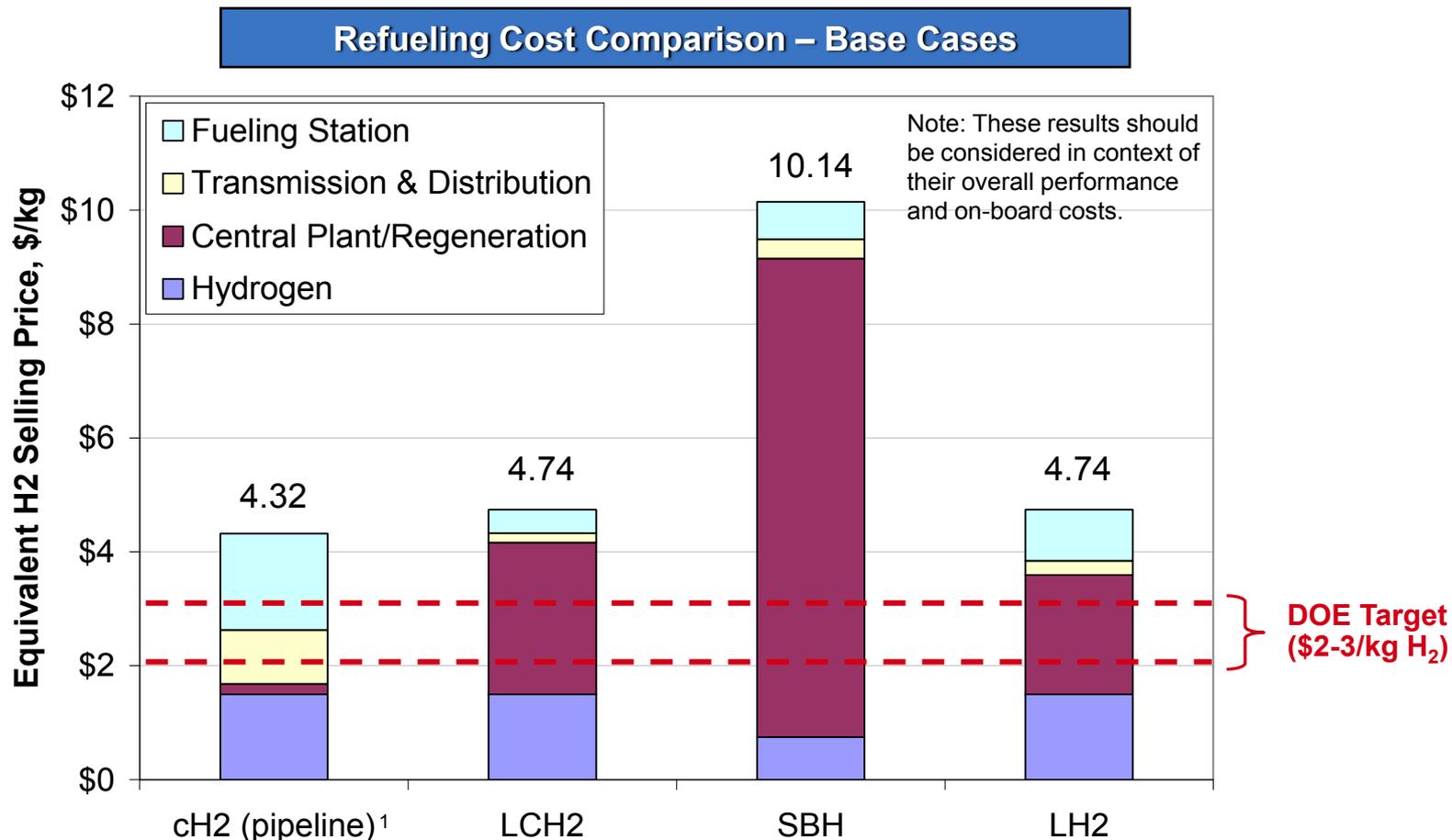


<sup>a</sup> The sodium alanate system requires high temp. waste heat for hydrogen desorption, otherwise the usable hydrogen capacity would be reduced.

<sup>b</sup> Normalizing the cryo-compressed and liquid H<sub>2</sub> systems for 5.6 kg of usable hydrogen results in system costs of ~\$20/kWh and ~\$14/kWh, respectively.

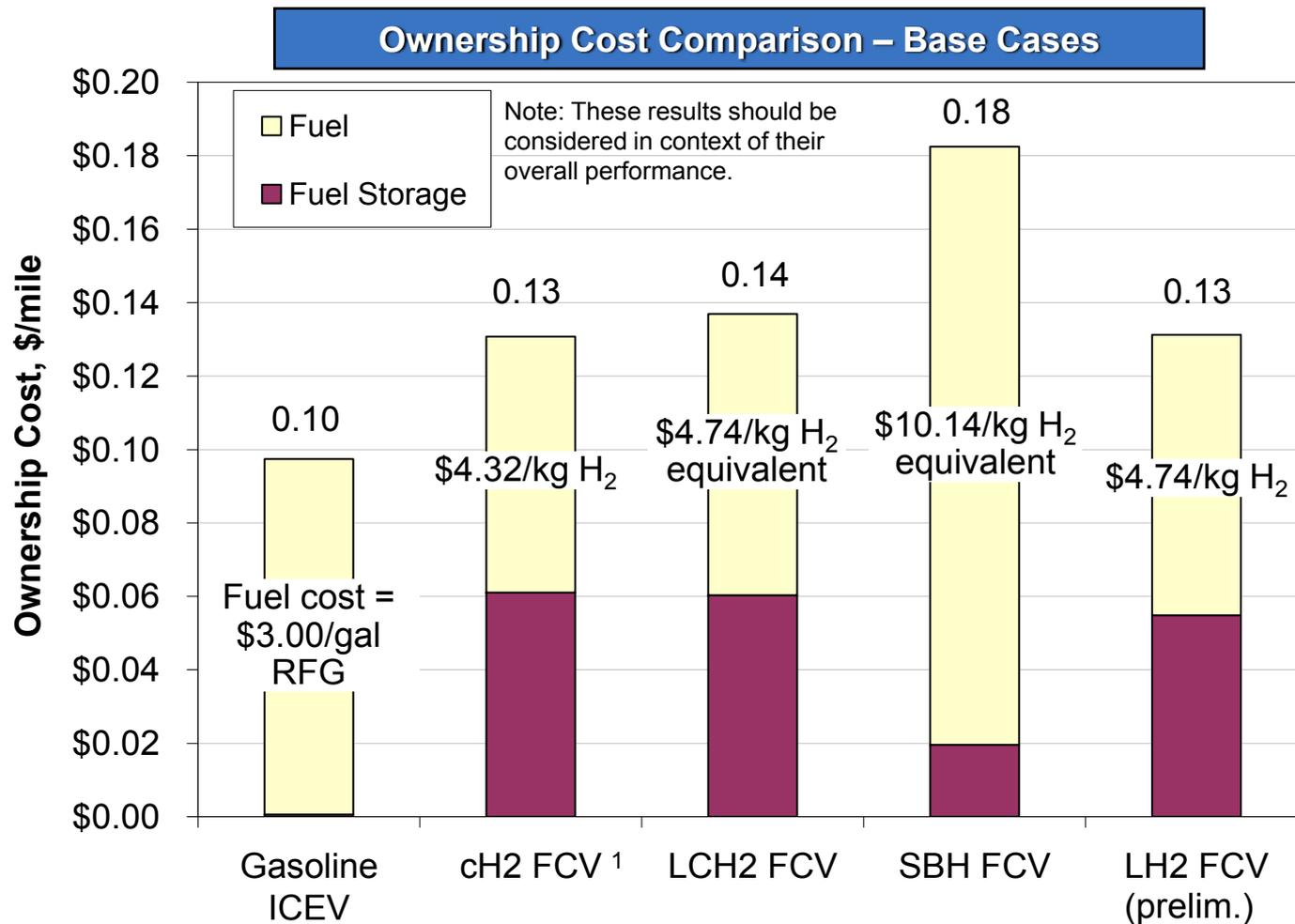


**Both compressed hydrogen (cH<sub>2</sub>) and LCH<sub>2</sub> refueling costs are projected to be 1.5-2.5 times more expensive than the DOE target range.**



<sup>1</sup> cH<sub>2</sub> option assumes compressed hydrogen pipeline delivery with 6,250 psi dispensing and 5,000-psi on-board storage system. Note: cH<sub>2</sub> and LH<sub>2</sub> results were calculated using the baseline delivery scenarios in HDSAM v2.06. LCH<sub>2</sub> and SBH results were calculated using a modified H2A Delivery Components Carrier Model v34. Detailed assumptions are presented in the Appendix.

**Fuel system ownership costs for the 5-ksi and LCH<sub>2</sub> systems are projected to be 35-40% more expensive than gasoline at \$3/gal.**



<sup>1</sup> cH<sub>2</sub> FCV option assumes compressed hydrogen pipeline delivery with 6,250 psi dispensing and 5,000-psi on-board storage system.  
 Note: Detailed assumptions are presented in the Appendix.



# Last year, we collaborated closely with ANL and numerous developers and other stakeholders participating in the DOE Grand Challenge.

- ◆ Argonne National Laboratory (ANL) - frequent email exchanges and monthly conference calls with DOE
  - LCH<sub>2</sub> and cH<sub>2</sub> on-board system design
  - LCH<sub>2</sub> and cH<sub>2</sub> on-board and off-board performance assessment
- ◆ H<sub>2</sub> Storage Centers of Excellence (SNL, LANL, PNNL, NREL, LLNL, SRNL) - participated in SSAWG and Novel Carrier meetings and some monthly conference calls as necessary
  - Reviewed assumptions and results for various technologies
- ◆ Independent projects and developers (APCI, R&H) - frequent email exchanges and regular conference calls throughout the cost assessment
  - LCH<sub>2</sub> on-board and off-board system designs
  - LCH<sub>2</sub> and AB off-board systems cost inputs
  - Reviewed assumptions and results for LCH<sub>2</sub> and AB results
- ◆ Stakeholders (Tech Teams, Quantum, SCI, Toray) – H<sub>2</sub> Delivery Tech Team meeting and frequent email exchanges and regular conference calls throughout the cost assessment
  - cH<sub>2</sub> on-board system cost inputs
  - Reviewed assumptions and results for updated cH<sub>2</sub> results
  - Tech Team reviewed R&H's AB off-board system cost inputs and results

## We have completed certain aspects of on-board and off-board evaluations and updates for nine hydrogen storage technologies.

Analysis To Date		cH <sub>2</sub>	Alanate	MgH <sub>2</sub>	SBH	Cryo-comp	LH <sub>2</sub>	AC	LCH <sub>2</sub>	AB
On-Board	Review developer estimates	√	√		√	√	√	√	√	
	Develop process flow diagrams and system energy balances	√	√		√	√	√		√	
	Independent performance assessment (wt, vol)	√	√		√	√	√*		√	
	Independent cost assessment	√	√		√	√	√*	WIP	√	
Off-Board	Review developer estimates	√		√	√	√	√		√	√
	Develop process flow diagrams and system energy balances	√		√	√				√	√
	Independent performance assessment (energy, GHG) <sup>a</sup>	√			√				√	
	Independent cost assessment	√			√		√		√	
Overall	Ownership cost projection	√			√		√		√	
	Solicit input on TIAX analysis	√	√		√	√*	√*	WIP	√	
	Analysis update	√			√	WIP	WIP			

\* Preliminary results under review.

<sup>a</sup> Work with ANL and H2A participants on separate WTT analysis tools.

■ = Not part of current SOW

WIP = Work in progress



### **For the remainder of the contract, we will focus on incorporating stakeholder feedback and submitting final reports for each technology.**

- ◆ Complete on-board cost assessments of liquid, cryo-compressed and AC options
  - Update previous results based on input from developers
  - Use latest compressed tank design and cost assumptions for cryo-compressed and AC
- ◆ Complete off-board cost assessment as requested by DOE and integrate with overall performance and on-board cost results
- ◆ Conduct cost assessment for new technologies (if any) selected by DOE with input from the Centers of Excellence and other developers after ANL performance assessment
  - Some technologies don't pass the performance filter and need additional R&D before a cost assessment makes sense
  - Those that pass the performance filter will be evaluated for on-board and off-board costs
- ◆ Continue to work with DOE, H2A, other analysis projects, developers, National Labs, and Tech Teams to revise and improve past system models
- ◆ Complete final reports with ANL for each detailed assessment to date
  - Draft final reports are already being written and/or reviewed for 5-ksi, 10-ksi and SBH
  - Start and complete reports for Sodium Alanate, Cryo-compressed, LH<sub>2</sub>, AC and LCH<sub>2</sub>
  - To the extent possible, well-to-wheel performance and lifecycle cost results will be presented in the final reports for each technology

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**Thank You**

**Questions?**

**Last year's objective was to evaluate a liquid hydrogen carrier (LCH<sub>2</sub>) and update our compressed hydrogen storage assessments.**

Objective	Technology Focus			
	2004-2006	2007	2008	2009
<b>On-Board Storage System Assessment</b>	<ul style="list-style-type: none"> <li>• Sodium Alanate</li> <li>• SBH</li> </ul>	<ul style="list-style-type: none"> <li>• Liquid H<sub>2</sub></li> <li>• Cryo-compressed H<sub>2</sub></li> </ul>	<ul style="list-style-type: none"> <li>• LCH<sub>2</sub></li> <li>• Compressed H<sub>2</sub> (5 and 10-ksi updates)</li> </ul>	<ul style="list-style-type: none"> <li>• AC</li> <li>• Liquid H<sub>2</sub> (update)</li> <li>• Cryo-compressed H<sub>2</sub> (update)</li> </ul>
<b>Off-Board Fuel Cycle Assessment</b>	<ul style="list-style-type: none"> <li>• Liquid H<sub>2</sub></li> <li>• Compressed H<sub>2</sub> (5 and 10-ksi)</li> </ul>	<ul style="list-style-type: none"> <li>• SBH</li> </ul>	<ul style="list-style-type: none"> <li>• LCH<sub>2</sub></li> </ul>	<ul style="list-style-type: none"> <li>• Ammonia Borane</li> <li>• Compressed H<sub>2</sub> (5 and 10-ksi updates)</li> <li>• Liquid H<sub>2</sub> (update)</li> </ul>

Note: Previously analyzed systems will continually be updated based on feedback and new information.

SBH = Sodium Borohydride, LCH<sub>2</sub> = Liquid Hydrogen Carrier, AC = Activated Carbon



**In addition, TIAX completed a high-level review of Rohm and Hass (R&H)'s cost assessment of ammonia borane (AB) regeneration and 1st fill production.**

- ◆ The goals of the review were as follows:
  - Validate R&H's implementation of the H2A Delivery Components Carrier Model for calculating the hydrogen equivalent cost for the AB regeneration and 1st fill production plants
  - Verify the underlying assumptions and cost inputs into the model
  - Check the energy and mass flows in the regeneration and 1st fill processes (to the extent possible)
- ◆ We reviewed two AB reports generated by R&H in February as well as other relevant reports
  - Evaluated all the process equipment and assumptions in addition to the implementation of these assumptions into the H2A Delivery Components Model supplied by R&H
  - The review was partially based on proprietary information received from R&H via the aforementioned reports as well as several conference calls
- ◆ R&H incorporated our feedback into their analysis and TIAX wrote a memo summarizing final comments and conclusions

**The cost of capital equipment, buildings, labor, utilities, etc. are included in our processing cost assessments.**

- ◆ Variable Cost Elements
  - Material
  - Direct Labor
  - Utility
- ◆ Operating Fixed Costs
  - Tooling & Fixtures
  - Maintenance
  - Overhead Labor
  - Cost of Operating Capital
- ◆ Non-Operating Fixed Costs
  - Equipment
  - Building
  - Cost of Non-Operating Capital

- ◆ Working Capital
  - Including materials, labor, utility, tooling and maintenance cost
  - Working capital period: 3 months

- ◆ Equipment
- ◆ Building

**We assume 100% debt financed with an annual interest rate of 15%, 10-year equipment life, and 25-year building life.**

The dehydrogenation reactor design was also based on information from APCI and ANL<sup>1,2</sup>.

System Element	Design Parameter	Base Case Value	Basis/Comment
<b>Dehydrogenation Reactor</b>	Type	Vertical, tubular trickle bed reactor	ANL <sup>2</sup>
	Heat of dehydrogenation	+51 kJ/mol H <sub>2</sub>	APCI <sup>1</sup> , ANL <sup>2</sup> ; =25 MJ/kg H <sub>2</sub>
	Catalyst	Pd on Li Aluminate	Dispersed wash-coat (thin-film) catalyst, 50 micron, 363 mm active length
	Catalyst concentration	4% wt. of substrate	
	Catalyst substrate	40-ppi Al-6101 foam	92% porosity, 224 kg/m <sup>3</sup> bulk density
	Conversion efficiency	95%	ANL <sup>2</sup>
	Liquid Hourly Space Velocity (LHSV)	20 h <sup>-1</sup>	ANL <sup>2</sup> ; H <sub>2</sub> volumetric flow rate/liter reactor volume
	Peak operating temp.	240-270 °C	ANL <sup>2</sup>
	Max. operating pressure	8 bar (116 psi)	ANL <sup>2</sup>
	HX tube material	Al-2219-T81	ANL <sup>2</sup> ; 40 tubes (11.1 mm OD, 0.8 mm wall, 400 mm length)
	Reactor vessel material	Al-2219-T81	ANL <sup>2</sup> ; 182 mm OD, 0.8 mm wall, 460 mm total length, 2.25 safety factor

<sup>1</sup> "Hydrogen Storage by Reversible Hydrogenation of Liquid-Phase Hydrogen Carriers", Cooper, A. and Pez., G, 2007 DOE Hydrogen Program Review

<sup>2</sup> "System Level Analysis of Hydrogen Storage Options", Ahluwalia, R.K. et al., 2007 DOE Hydrogen Program Review, May 2007

## LCH<sub>2</sub> Design Assumptions Continued

System Element	Design Parameter	Base Case Value	Basis/Comment
<b>H<sub>2</sub> Buffer Storage Tank</b>	Material	Al-2219-T81	ANL <sup>2</sup> ; (249 mm OD, 0.5 mm wall, 744 mm total length, 2.25 safety factor)
	Peak Operating Temp	80 °C	ANL <sup>2</sup>
	Max. Operating Pressure	8 bar (116 psi)	ANL <sup>2</sup>
	Tank capacity	20 g H <sub>2</sub>	ANL <sup>2</sup>
<b>HEX Burner</b>	Burner type	H <sub>2</sub> /air (non-catalytic)	ANL <sup>2</sup> ; 5% excess O <sub>2</sub> , 1100 °C combustion products' exit temperature
	Burner fuel	32.3% by weight of stored H <sub>2</sub>	
	Burner firing rate	82 kW (280,000 Btu/h)	
	HX Type	Counterflow Microchannel	ANL <sup>2</sup> ; HTF=XCeItherm® 600, 100 °C approach temp., 310 microchannels (14.1 mm x 0.9 mm x 363 mm)
	HX Material	Inconel 600	
<b>H<sub>2</sub> Cooler</b>	HX Type	Counterflow Microchannel	ANL <sup>2</sup> ; T <sub>outlet</sub> = 80 °C, 90 microchannels (10.6 mm x 1.4 mm x 165 mm)
	HX Material	SS316	
<b>Recuperator</b>	HX Type	Counterflow Microchannel	ANL <sup>2</sup> ; T <sub>LCH<sub>2</sub></sub> = T <sub>R</sub> -10 °C, 610 microchannels (10.1 mm x 0.6 mm x 263 mm)
	HX Material	SS316	

<sup>1</sup> "Hydrogen Storage by Reversible Hydrogenation of Liquid-Phase Hydrogen Carriers", Cooper, A. and Pez., G, 2007 DOE Hydrogen Program Review

<sup>2</sup> "System Level Analysis of Hydrogen Storage Options", Ahluwalia, R.K. et al., 2007 DOE Hydrogen Program Review, May 2007

## LCH<sub>2</sub> Design Assumptions Continued

System Element	Design Parameter	Base Case Value	Basis
<b>HTF Pump</b>	Working fluid	XCelTherm® 600	ANL <sup>2</sup>
	Operating Temp	320 °C	
	Pressure Head	1 bar (15 psi)	
	Density	850 kg/m <sup>3</sup>	
	Flow rate	458 Liter/min (6.5 kg/s)	
<b>LCH<sub>2</sub> Pump</b>	Working fluid	LCH <sub>2</sub>	ANL <sup>2</sup>
	Operating Temp	70 °C	
	Pressure Head	8 bar (116 psi)	
	Density	1200 kg/m <sup>3</sup>	
	Flow rate	2.65 Liter/min (0.053 kg/s)	

<sup>1</sup> "Hydrogen Storage by Reversible Hydrogenation of Liquid-Phase Hydrogen Carriers", Cooper, A. and Pez., G, 2007 DOE Hydrogen Program Review

<sup>2</sup> "System Level Analysis of Hydrogen Storage Options", Ahluwalia, R.K. et al., 2007 DOE Hydrogen Program Review, May 2007

**We used Year 2008 prices for the key raw materials, which are listed below. Subsequently, we deflated all material prices by 9.27% to Year 2005 USD.**

System Element	Raw Material	Base Case Price (Year 2008 USD)	Basis/Comment
Media	N-ethylcarbazole	\$7/gal	APCI; \$2-12/gal range; consistent with TIAX off-board LCH <sub>2</sub> storage system assessment
LCH <sub>2</sub> /LC Storage Tank	HDPE	\$1.83/kg	Plastics Technology, May 2008, pg. 95
Dehydrogenation Reactor	Pd catalyst	\$14/g (\$436/tr.oz.)	www.metalprices.com; June, 2008
	Li Aluminate	\$48/kg	<a href="https://www.sigmaaldrich.com/catalog/search/ProductDetail?ProdNo=336637&amp;Brand=ALDRICH">https://www.sigmaaldrich.com/catalog/search/ProductDetail?ProdNo=336637&amp;Brand=ALDRICH</a>
	Al-6101	\$2.8/kg	LME Al alloy, 15-month avg., June 2008
	Al-2219-T81	\$3.7/kg	<a href="http://www.steelforge.com">http://www.steelforge.com</a> , June 2008
	HTF (XCelTherm® 600)	\$8/gal	RadCo Industries, Inc., June 2008
HEX Burner	Inconel 600	\$16.5/kg	www.metalprices.com; June, 2008
H <sub>2</sub> Cooler, Recuperator	SS316	\$8/kg	www.metalprices.com; June, 2008, 1-year avg.

**We based the cost of purchased components on vendor quotes/catalog prices, using our judgment to adjust for high-volume production.**

Purchased Component	Weight (kg)	Volume (L)	Base Case Cost (\$)	Basis/Comment
HTF Pump	40	30	\$400	0.4X McMaster-Carr catalog price; ANL1: XCelTherm® 600, 458 L/min, 320 °C, ΔP=1 bar
LCH <sub>2</sub> Pump	20	10	\$200	0.4X McMaster-Carr catalog price; ANL1: LCH <sub>2</sub> , 2.65 L/min, 70 °C, ΔP=8 bar
H <sub>2</sub> /air Non-catalytic Burner	2	1	\$400	0.4X McMaster-Carr catalog price \$1,000 for NG burner, 180,000 Btu/h; ANL1: 82 kW, 5% excess O <sub>2</sub> , Inconel
H <sub>2</sub> Blower	2.0	5	\$18	0.5X Modine OEM \$37 not including tooling and capital cost markup 1.2
Coagulating filter	1.8	0.8	\$21	Same as for SBH system; 0.2X retail \$105
LCH <sub>2</sub> Tank Heater	0.1	0.0	\$4	Bottom-up costing using Boothroyd-Dewhurst DFMA® software, with 1.5X markup for component supplier overhead and profit
Piping & Fittings	7	3	\$72	
Sensors & Controls	0.0	0.0	\$30	
Valves & Connectors	3	2	\$105	
Pressure Regulators	1	1	\$44	

<sup>1</sup> "System Level Analysis of Hydrogen Storage Options", Ahluwalia, R.K. et al., 2007 DOE Hydrogen Program Review, May 2007

**We performed bottom-up costing (i.e., raw materials, process flow charts) on all other components.**

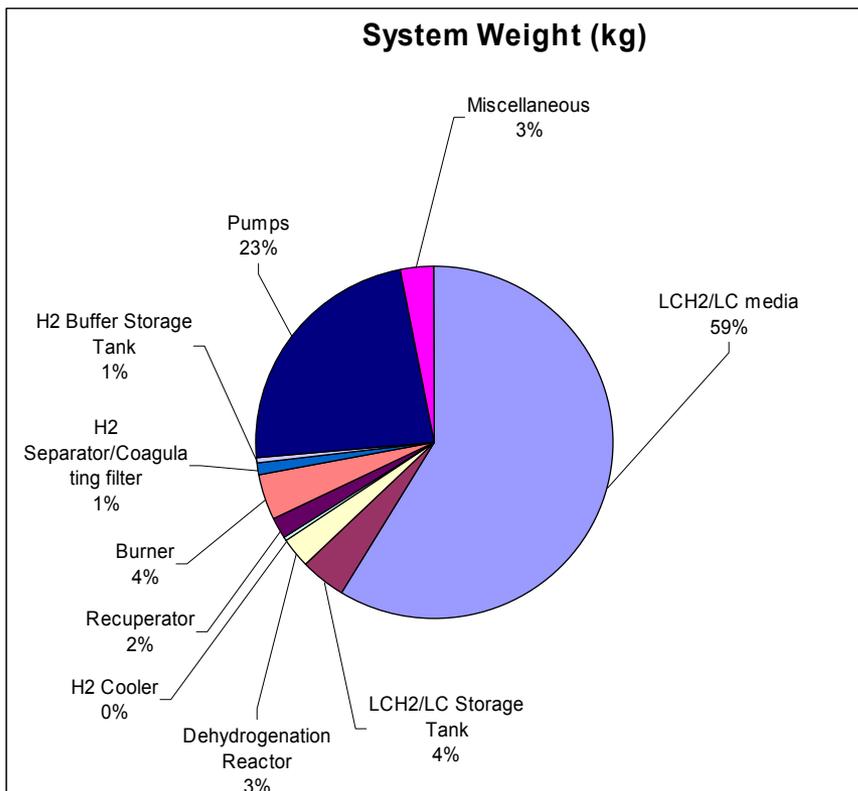


**Processing cost makes up just ~5% of the total system cost due to the high production volume assumption and large fraction of purchased components.**

On-board System Cost Breakout Liquid Hydrogen Carrier – 5.6 kg H <sub>2</sub>	Material, \$	Processing, \$	Processing Fraction
LCH <sub>2</sub> /LC Media <sup>1</sup>	210	(purchased)	0.0%
LCH <sub>2</sub> /LC Storage Tank	55	10	15.4%
<b>Dehydrogenation Reactor</b>	<b>1,008</b>	<b>37</b>	<b>3.5%</b>
- Pd Catalyst	916	(purchased)	0.0%
- Li Aluminate	76	(purchased)	0.0%
- Al-6101 foam substrate	4	19	82.6%
- Reactor Vessel (Al-2219-T81)	3	2	40.0%
- HX tubes (Al-2219-T81)	4	16	80.0%
- Other (HTF, insulation, fittings)	5	(purchased)	0.0%
H <sub>2</sub> Cooler	6	24	80%
Recuperator	36	24	40%
<b>Burner</b>	<b>510</b>	<b>36</b>	<b>6.6%</b>
- Microchannel HX	92	36	28.1%
- H <sub>2</sub> /air non-catalytic burner	400	(purchased)	0.0%
- H <sub>2</sub> blower	18	(purchased)	0.0%
H <sub>2</sub> Separator/Coagulating filter	30	7	18.9%
H <sub>2</sub> Buffer Storage Tank	7	0.5	6.7%
<b>Pumps</b>	<b>600</b>	<b>(purchased)</b>	<b>0.0%</b>
- HTF pump	400	(purchased)	0.0%
- LCH <sub>2</sub> pump	200	(purchased)	0.0%
Miscellaneous	251	(purchased)	0.0%
Final Assembly & Inspection	0	17	100.0%
<b>Total Factory Cost</b>	<b>2,713</b>	<b>156</b>	<b>5.4%</b>

<sup>1</sup> Cost is based on \$7/gal LCH<sub>2</sub>, consistent with TIAX off-board LCH<sub>2</sub> storage system assessment, which is based on input from APCI.

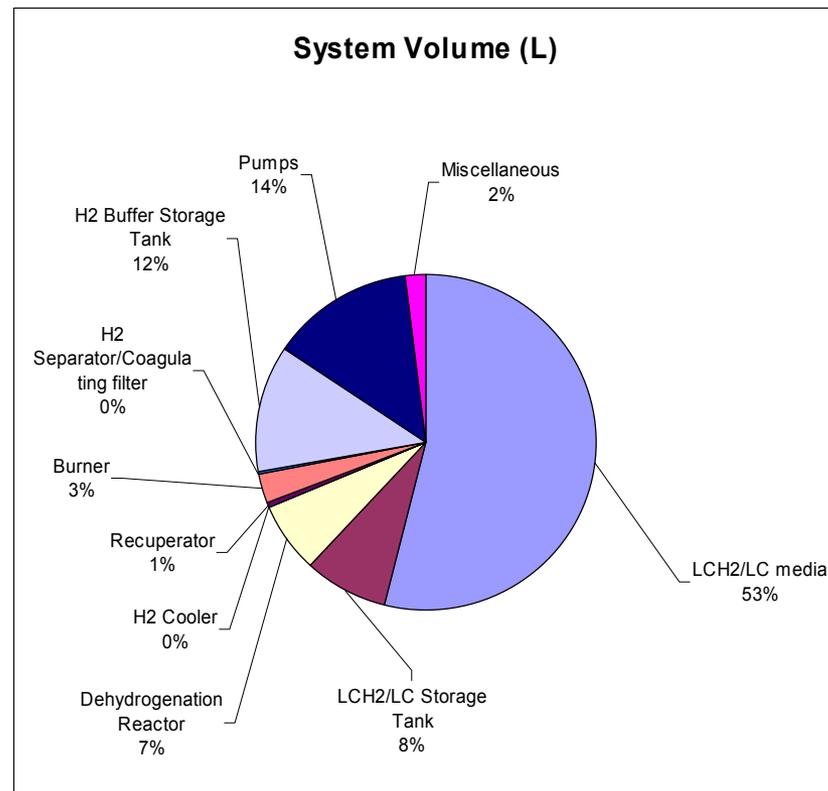
**We estimate the system weight to be 256 kg (2.2% wt.% H<sub>2</sub>) and system volume to be 293 L (19 g H<sub>2</sub>/L), primarily driven by the LCH<sub>2</sub> media.**



**System Weight = 256 kg**

2.2 wt% based on 5.6 kg usable H<sub>2</sub> (8.7 kg stored H<sub>2</sub>)

Compare to ANL estimate<sup>1</sup> = 2.8% wt.% H<sub>2</sub> for 10 kg stored H<sub>2</sub>



**System Volume = 293 L**

19 g H<sub>2</sub>/L based on 5.6 kg usable H<sub>2</sub> (8.7 kg stored H<sub>2</sub>)

Compare to ANL estimate<sup>1</sup> = 23 g H<sub>2</sub>/L for 10 kg stored H<sub>2</sub>

Note: A trade-off study was not performed on the size/cost of the pumps versus size/cost of the reactor sub-system and burner.

<sup>1</sup> "System Level Analysis of Hydrogen Storage Options", Ahluwalia, R.K. et al., 2007 DOE Hydrogen Program Review, May 2007

**The chemical hydride (LCH<sub>2</sub> and SBH) off-board cost results were calculated using a modified version of the Delivery Components Carrier Model v34.**

- ◆ Most financial assumptions are maintained from the original H2A Delivery Components Model
- ◆ New calculation tabs were added as part of the DOE Delivery Project for novel carriers, resulting in the H2A Deliver Components Carrier Model v34
  - Regeneration – calculates material regeneration costs based on capital and operating costs of a central plant and the storage capacity of the material
  - Storage Terminal – calculates required storage for fresh and spent materials
  - Trucking – calculates trucking costs for all novel carriers
  - Fueling Station – calculates fueling station costs for novel carrier storage and vehicle fueling
- ◆ These new calculation tabs were populated with inputs based on industry and developer feedback specifically for LCH<sub>2</sub> and SBH
  - TIAX made initial estimates consistent with H2A methodology
  - Model and estimates were reviewed with developers
  - Model inputs and results were updated

**Capital cost estimates are derived from developer feedback and baseline H2A model assumptions.**

Regeneration Plant Capital Equipment	Installed Cost (\$millions)	Basis
Carrier Material	\$285	Personal communication with APCI, 2008
Indirect Capital (permitting, project contingency, engineering, site prep, land)	\$166	H2A Baseline
Storage (Including quarantine)	\$41.7	Personal communication with APCI, 2008
Piping & Instrumentation	\$25.7	Personal communication with APCI, 2008
Catalyst	\$21.3	Personal communication with APCI, 2008
Compressors	\$14.8	H2A Baseline
Pumps	\$6.8	Personal communication with APCI, 2008
Reactor	\$1.5	Personal communication with APCI, 2008
Heat Exchangers	\$1.4	Personal communication with APCI, 2008
Distillation	\$0.2	Personal communication with APCI, 2008
<b>Total</b>	<b>\$564</b>	

**The ability of the liquid carrier to be transported in relatively standard, insulated tank trucks makes for cost efficient transportation.**

- ◆ Transport capacity: determined by the liquid carrier yield (3.7 wt% net) and the mass of material that can be transported within an insulated aluminum trailer (24,750 kg GVW)
- ◆ Insulation: will be able to maintain the temperature of the carrier for up to 1 day
- ◆ Trailer cost: \$90,000 based on quotes from Heil and Polar trailer companies
- ◆ Loading/unloading time: 1.5 hrs combined (trailer unloads hydrogenated carrier and picks up dehydrogenated carrier)
- ◆ Baseline H2A assumptions include:

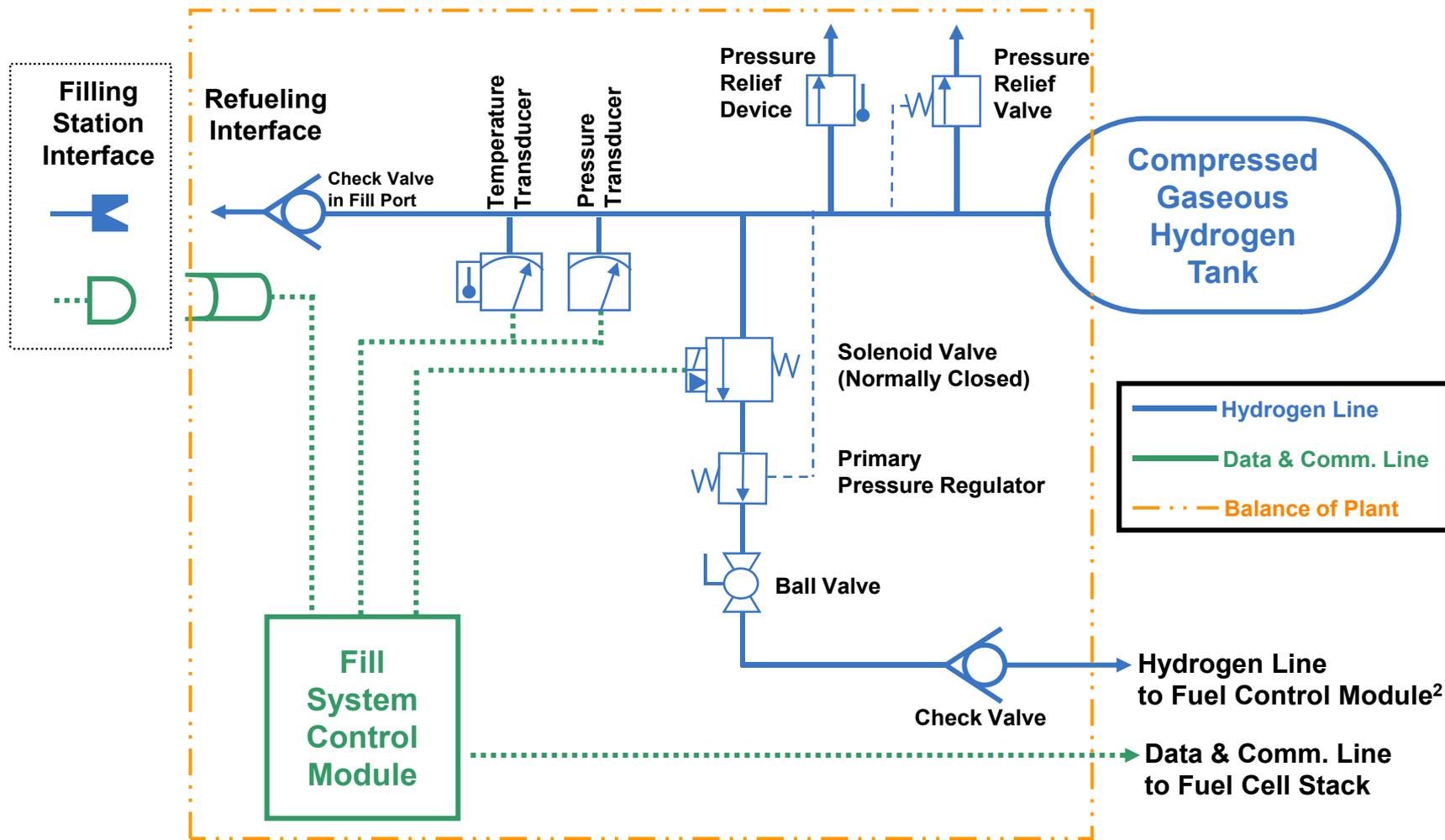
H2A Delivery Assumption	Value
Round trip delivery distance	160 km
Delivery labor rate	\$50
Truck capital cost	\$75,000
Fuel cost	0.44 \$(2005)/L



**This analysis assumes the fueling station receives the liquid carrier via tanker trucks where the carrier is stored and dispensed to vehicles for on-board dehydrogenation.**

- ◆ All components (e.g., storage tanks, pumps, dispensers) are specified according to previously established methods for chemical hydrogen systems
- ◆ On-site storage in each of the hydrogenated and spent carrier tanks is equal to 1.5 truck deliveries
- ◆ Overall cost includes enough carrier material to fill 1/3 of the hydrogenated carrier tank and the full spent carrier tank
- ◆ Electricity consumption due to carrier pumping and other miscellaneous loads are the same as for sodium borohydride (SBH) = 0.50 kWh/kg
- ◆ A range of labor costs were used: \$7.75/hr (minimum wage in CA) - \$15/hr, with the baseline value of \$10/hr

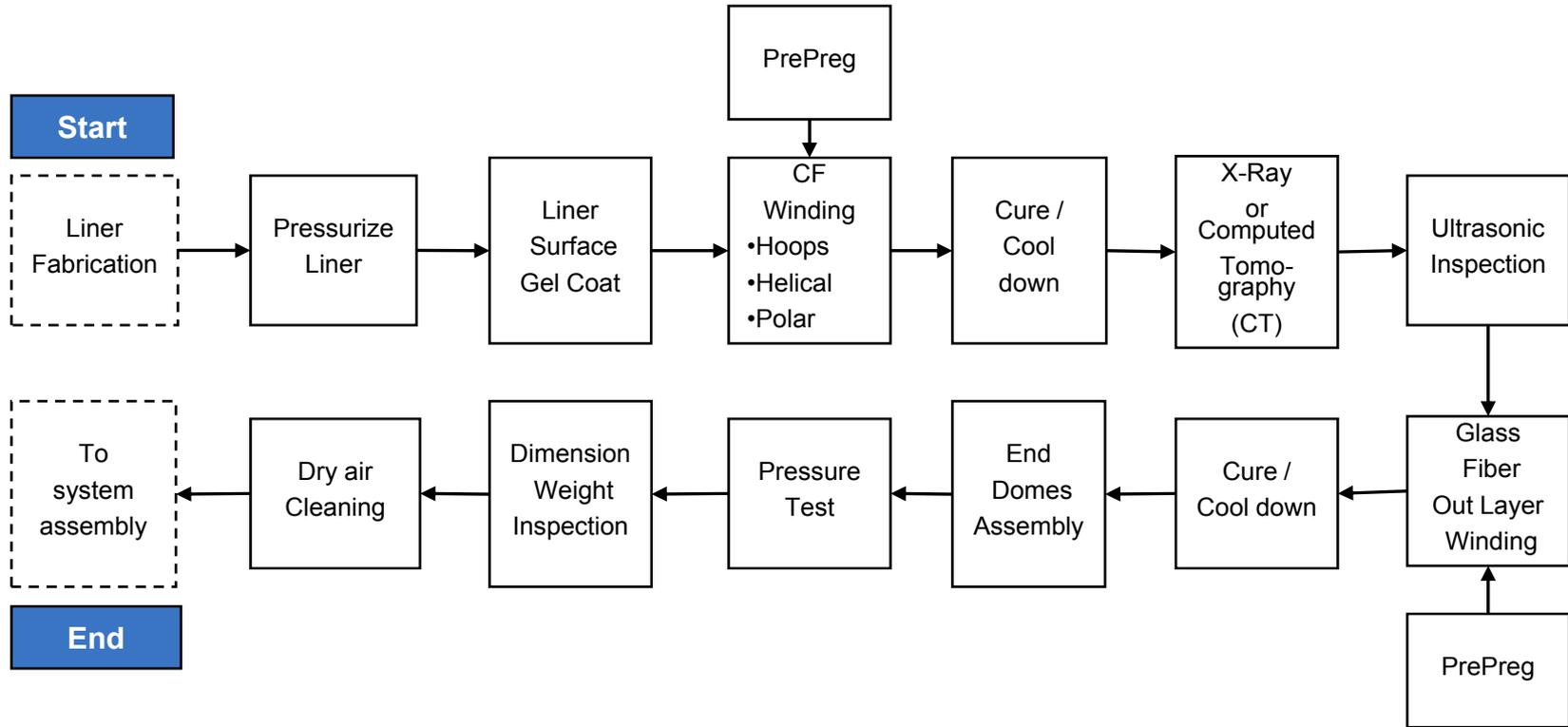
The system schematic<sup>1</sup> and bill of materials for the compressed systems were generated through discussions with tank developers.



<sup>1</sup> Schematic based on the requirements defined in the draft European regulation "Hydrogen Vehicles: On-board Storage Systems" and US Patent 6,041,762.

<sup>2</sup> Secondary Pressure Regulator located in Fuel Control Module.

The process for manufacturing wound composite tanks is well established from the Compressed Natural Gas Industry.



\*Note that about 60 winding machines would be required for 500,000 5,000-psi tanks per year; about 100 machines would be required for 10,000-psi tanks.

**We updated the carbon fiber composite calculations, which can significantly effect the overall weight and cost results.**

- ◆ End dome shape and thickness modeled using composite pressure vessel algorithm<sup>1</sup>
  - Combination of hoop and helical windings assumed, with only helical windings on the end domes; ratio of hoop/helical windings equal to 1.8
  - Non-uniform end dome thickness; thickest at dome peak (exit hole)
  - Model yields carbon fiber weight calculations consistent with Quantum’s models
- ◆ Carbon fiber composite requirement<sup>2</sup> for the rest of the tank also changed due to changes to the base case assumptions:
  - Safety factor changed to 2.35 from 2.25 and applied to nominal tank pressure (i.e., 5,000 and 10,000 psi) rather than max filling over pressure (i.e., 6,250 and 12,500 psi)
  - Carbon fiber composite tensile strength updated to 2,550 MPa from 2,940 MPa

2008 Updated Base Case Assumptions	5,000-psi	% Change '08/'06	10,000-psi	% Change '08/'06
Cylinder Composite Thickness, mm	14.3	19%	30.8	18%
Total Composite Weight, kg	51.7	8%	81.8	2%

<sup>1</sup> “Mechanics and Analysis of Composite Materials”, Vasiliev and Morozov, New York: Elsevier Science, 2001.

<sup>2</sup> Other minor changes include assumptions for tank diameter and minimum tank pressure.



**We based the cost of purchased BOP components on vendor quotes/catalog prices, using our judgment to adjust for high-volume production.**

BOP Component	5,000-psi System			10,000-psi System		
	Weight (kg)	Volume (L)	Base Case Cost (\$)	Weight (kg)	Volume (L)	Base Case Cost (\$)
Regulator	2	1	250	3	1.3	350
Valves	2.5	1	200	3.5	1.5	250
Fittings, Bosses & Pipe	7	1	140	7	1	160
Fill Port	0.5	1	80	0.5	1	100
Miscellaneous	2	1	50	2	1	70
<b>Total</b>	14	5	720	16	6	930

**We performed bottom-up costing (i.e., raw materials plus processing costs) on all other components.**

Raw Material	Base Case Price (\$/kg)	Basis/Comment
Hydrogen	3.0	Consistent with DOE H <sub>2</sub> delivery target
T700S CF Prepreg	36.6	Discussion w/ Toray (2007) re: T700S fiber (\$10-\$16/lb, \$13/lb base case) 1.27 prepreg/fiber ratio (DuVall 2001)
HDPE Liner	1.8	Plastics Technology, 2008
Glass Fiber Prepreg	5	Discussions with AGY, 2007 for non-structural fiber glass
Foam End Caps	7	Plastics Technology

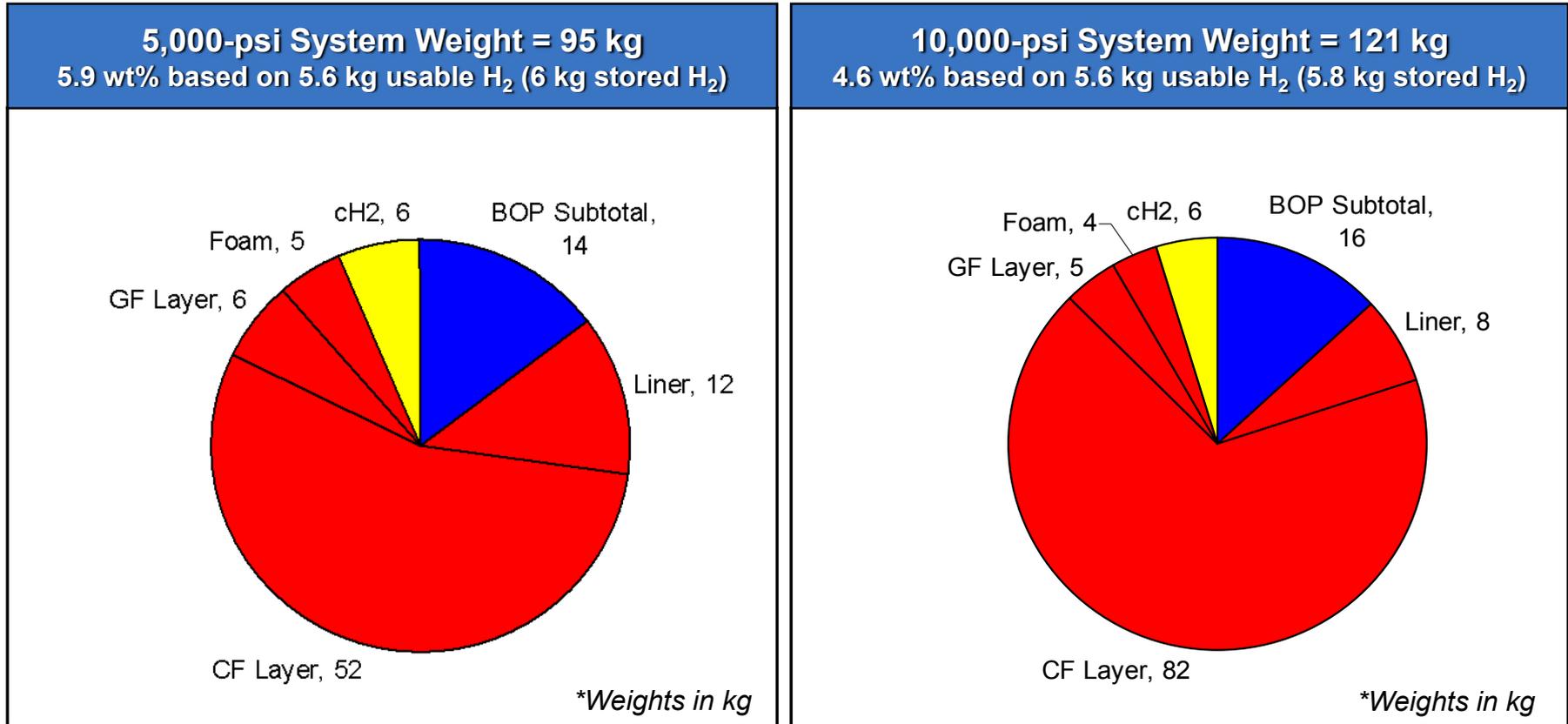


**Processing cost makes up just ~5% of the total system cost due to the high production volume assumption and large fraction of purchased components.**

On-board System Cost Breakout Compressed Hydrogen Base Case – 5.6 kg H <sub>2</sub>	5,000-psi			10,000-psi		
	Material, \$	Processing, \$	Processing Fraction	Material, \$	Processing, \$	Processing Fraction
Hydrogen	18	(purchased)	-	18	(purchased)	-
Pressure Vessel	2,056	98	5%	3,187	138	4%
- Liner	21	11	35%	14	10	41%
- Carbon Fiber Layer	1,972	78	4%	3,117	120	4%
- Glass Fiber Layer	32	7	18%	25	6	19%
- Foam	32	2	6%	30	2	6%
Regulator	250	(purchased)	-	350	(purchased)	-
Valves	200	(purchased)	-	250	(purchased)	-
Fittings, Bosses & Pipe	130	(purchased)	-	160	(purchased)	-
Fill Port	80	(purchased)	-	100	(purchased)	-
Miscellaneous	50	(purchased)	-	70	(purchased)	-
Final Assembly & Inspection	-	36	-	-	36	-
<b>Total Factory Cost</b>	<b>2,784</b>	<b>134</b>	<b>5%</b>	<b>4,135</b>	<b>174</b>	<b>4%</b>

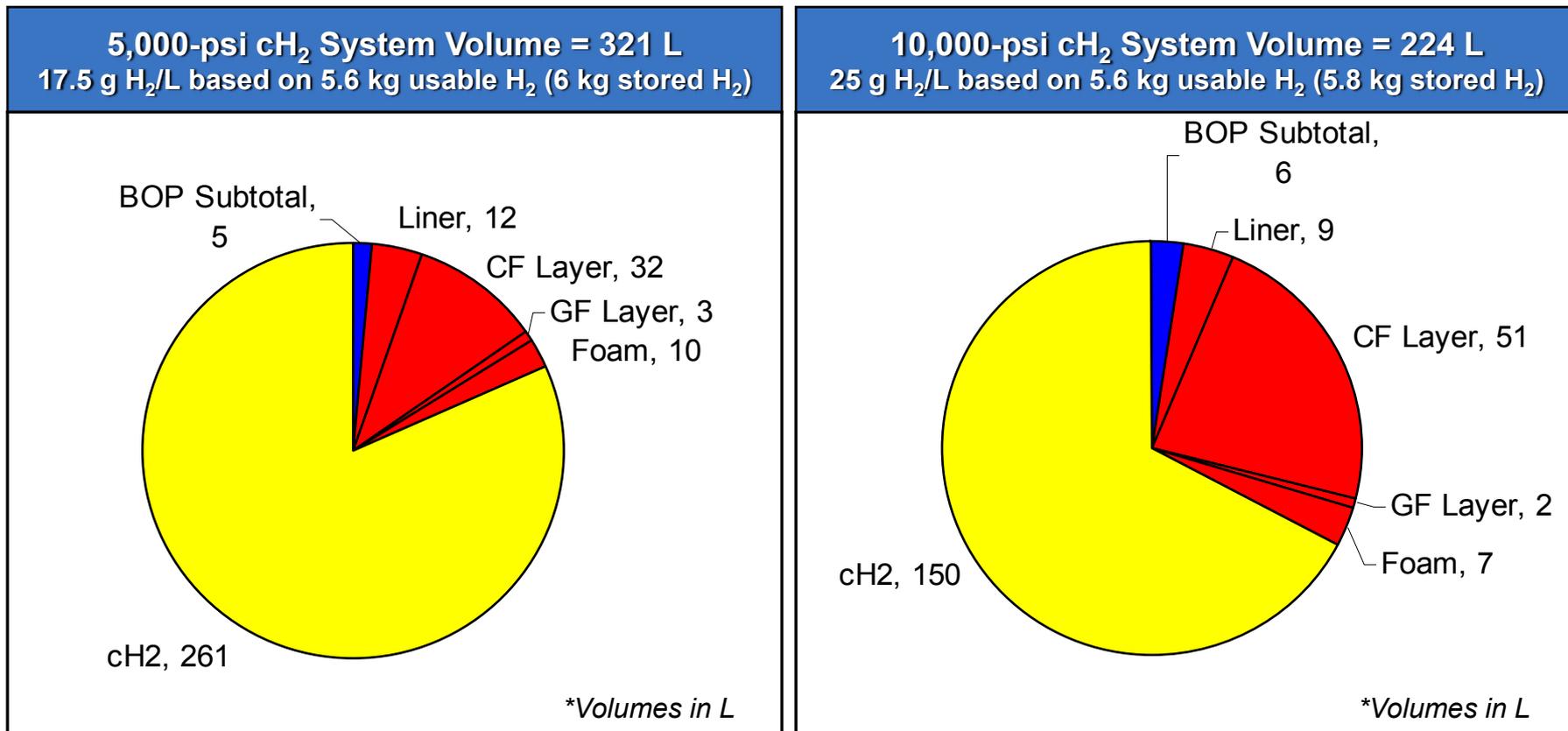


For the baseline conditions, CF composite accounts for 55% of the total weight of the 5,000-psi system and about 70% of the 10,000-psi system.



The gravimetric capacity of the 10,000-psi tank system is lower, despite the higher density of the stored H<sub>2</sub>, due to the additional CF composite required.

**For the baseline conditions, the stored hydrogen accounts for 80% of the total volume of the 5,000-psi system and about 70% of the 10,000-psi system.**



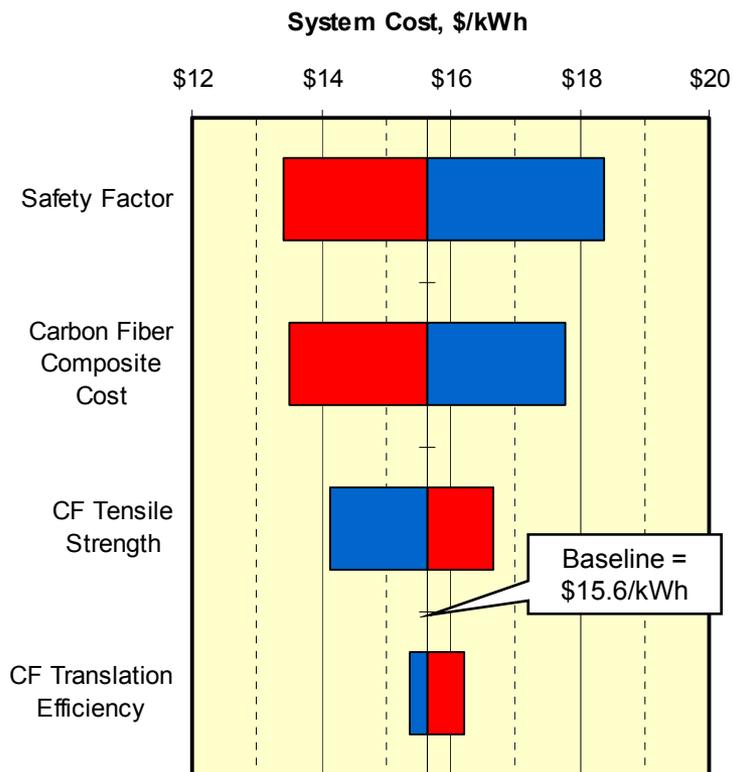
Note: Volume results do not include void spaces between components (i.e., no packing factor was applied).

**The volume of the hydrogen alone fails to meet the 2010 targets of 45 g H<sub>2</sub>/L (124 L for 5.6 kg H<sub>2</sub>).**

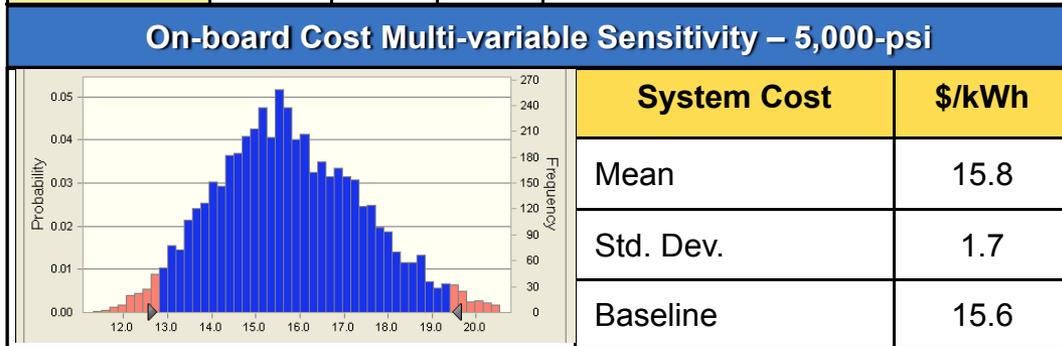


The range of uncertainty for the 5,000-psi tank’s CF cost and safety factor have the biggest impact on the base case cost estimate (roughly 15-20% each).

**On-board Cost Sensitivity – 5,000-psi (5.6 kg H<sub>2</sub>), \$/kWh**



Key Sensitivity Parameters	On-board Cost Sensitivity – 5,000-psi			
	Base	Min	Max	Basis/Comment
Safety Factor	2.35	1.80	3.0	<ul style="list-style-type: none"> <li>◆ Base case is based on EIHP Rev 12b design criteria</li> <li>◆ Min and Max based on discussions with Quantum and Dynatek (2005)</li> </ul>
CF Prepreg (Fiber & Matrix) Cost (\$/lb)	16.6	12.8	20.4	<ul style="list-style-type: none"> <li>◆ Based on discussion w/ Toray (2007) re: T700S fiber (\$10-\$16/lb, \$13/lb base case)</li> <li>◆ 1.27 prepreg/fiber ratio (DuVall 2001)</li> </ul>
CF Tensile Strength (MPa)	2,550	2,300	3,000	<ul style="list-style-type: none"> <li>◆ Base case from Toray T700S data sheet (2007)</li> <li>◆ Max calculated from fiber volume fraction (60%) and fiber strength (4,900 MPa)</li> <li>◆ Min assumes 10% decrease from base case</li> </ul>
CF Translation Strength (%)	81.5%	78%	85%	<ul style="list-style-type: none"> <li>◆ Based on Quantum (2005) for 5,000-psi CF tanks</li> </ul>

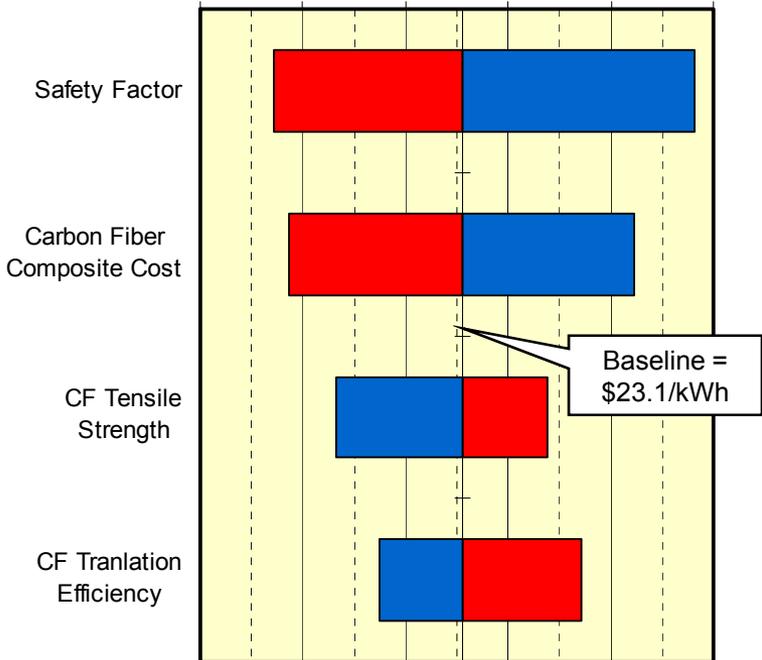


**Likewise, variability in the parameters affecting CF requirements can significantly affect the overall cost of the 10,000-psi tank system.**

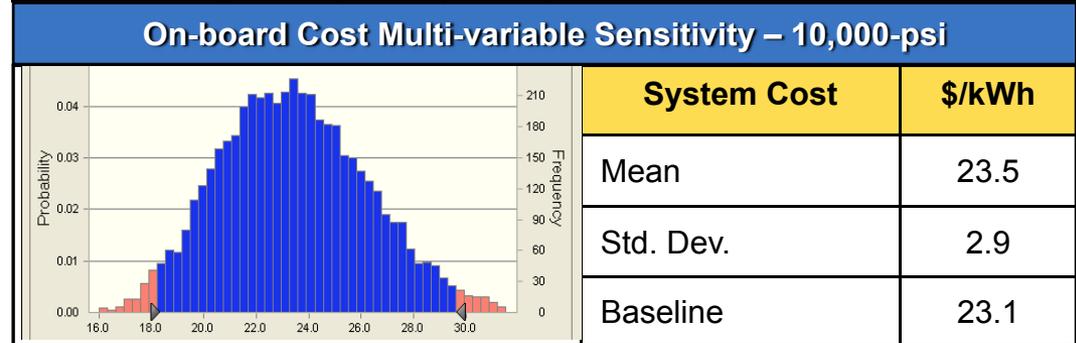
**On-board Cost Sensitivity – 10,000-psi (5.6 kg H<sub>2</sub>), \$/kWh**

System Cost, \$/kWh

\$18    \$20    \$22    \$24    \$26    \$28



Key Sensitivity Parameters	On-board Cost Sensitivity - 10,000-psi			
	Base	Min	Max	Basis/Comment
Safety Factor	2.35	1.80	3.0	<ul style="list-style-type: none"> <li>◆ Base case is based on EIHP Rev 12b design criteria</li> <li>◆ Min and Max based on discussions with Quantum and Dynatek (2005)</li> </ul>
CF Prepreg (Fiber & Matrix) Cost (\$/lb)	16.6	12.8	20.4	<ul style="list-style-type: none"> <li>◆ Based on discussion w/ Toray (2007) re: T700S fiber (\$10-\$16/lb, \$13/lb base case)</li> <li>◆ 1.27 prepreg/fiber ratio (DuVall 2001)</li> </ul>
CF Translation Strength (%)	63%	55%	70%	◆ Based on Quantum (2005) for 10,000-psi CF tanks
CF Tensile Strength (MPa)	2,550	2,300	3,000	<ul style="list-style-type: none"> <li>◆ Base case from Toray T700S data sheet (2007)</li> <li>◆ Max calculated from fiber volume fraction (60%) and fiber strength (4,900 MPa)</li> <li>◆ Min assumes 10% decrease from base case</li> </ul>



**5,000 and 10,000-psi system cost, weight and volume decreased (grav. and vol. capacities increased) due to revised assumptions from the last Merit Review.**

- ◆ The key change resulting in the decreases was that the tank safety factor was applied to the *nominal* tank pressure (i.e., 5,000 and 10,000 psi) rather than *max. filling* over pressure (i.e., 6,250 and 12,500 psi) based on new/contradictory information from industry
- ◆ Changing the tank end dome shape based on ANL’s latest performance analysis, which uses a composite pressure vessel algorithm<sup>1</sup>, also resulting in decreases
- ◆ Changing the carbon fiber composite tensile strength from 2,940 to 2,550 MPa to be consistent with ANL’s latest performance analysis partially offset the above adjustments
- ◆ There were several other less significant changes that were made based on the latest industry feedback<sup>2</sup> or to match the latest ANL assumptions

2009 Updated Results and % Change '09/'08 AMR	5,000 psi System		10,000 psi System	
	Base Case	% Change	Base Case	% Change
System Cost, \$/kWh	15.6	-9%	23.1	-13%
Gravimetric Capacity, wt%	5.9	11%	4.7	18%
Volumetric Capacity, g H <sub>2</sub> /L	17.5	3%	25.0	9%

<sup>1</sup> “Mechanics and Analysis of Composite Materials”, Vasiliev and Morozov, New York: Elsevier Science, 2001

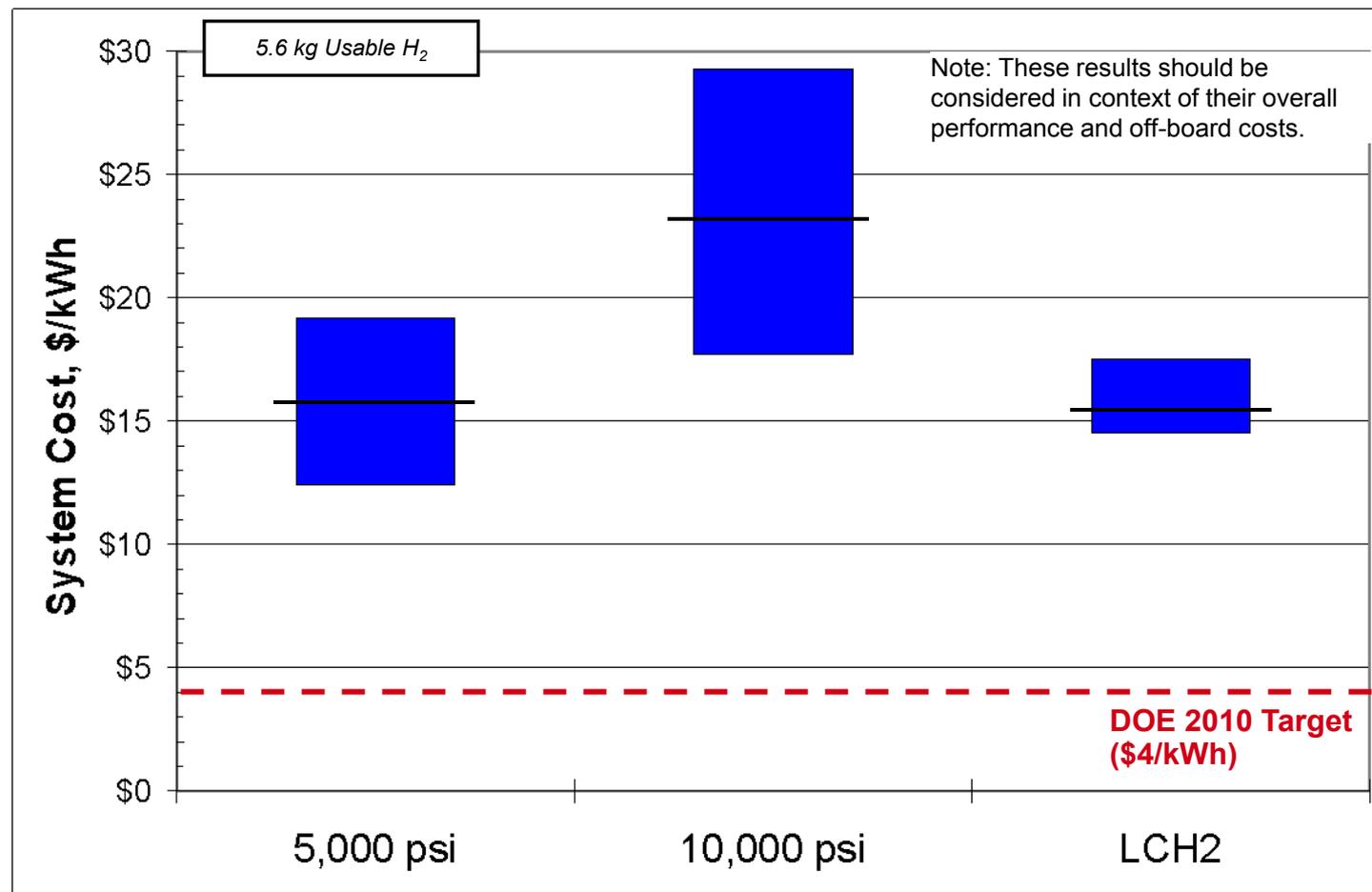
<sup>2</sup> For example, the tank empty pressure assumption changed from 400 psi for 5,000-psi tanks and 200 psi for 10,000-psi tanks to 290 psi for both.



The compressed (cH<sub>2</sub>) and liquid hydrogen (LH<sub>2</sub>) off-board cost results were calculated using the baseline delivery scenarios in HDSAM v2.06.

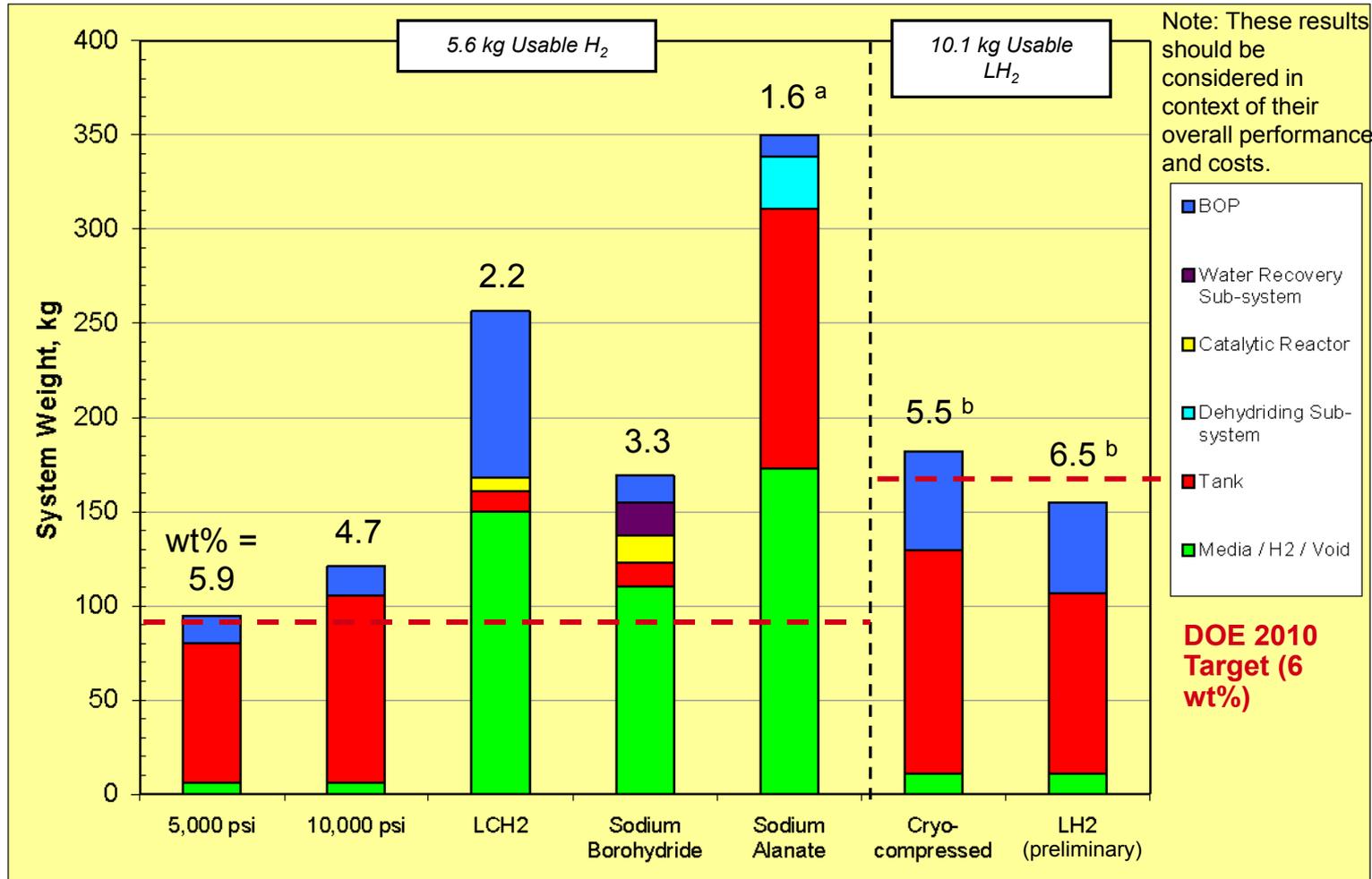
HDSAM Delivery Scenario Assumptions	cH <sub>2</sub>	LH <sub>2</sub>
Hydrogen Market	Urban	Urban
Market Penetration	30%	30%
City Selection	Indianapolis, IN (~1.2M people)	Indianapolis, IN (~1.2M people)
Transmission/Distribution Mode	Compressed gas pipeline	Cryogenic liquid trucks
Plant Outage and Summer Peak Storage	Geologic	Cryogenic liquid tanks
Refueling Station Size	1,000 kg/day	1,000 kg/day
Assumed On-board Storage System	5,000 psi compressed	Cryogenic liquid

**None of the on-board system designs evaluated last year are expected to meet the DOE 2010 cost target based on the sensitivity analyses<sup>1</sup>.**



<sup>1</sup> Based on the range of likely cost and performance values. Range is defined here as the mean plus/minus two standard deviations (~95% confidence).

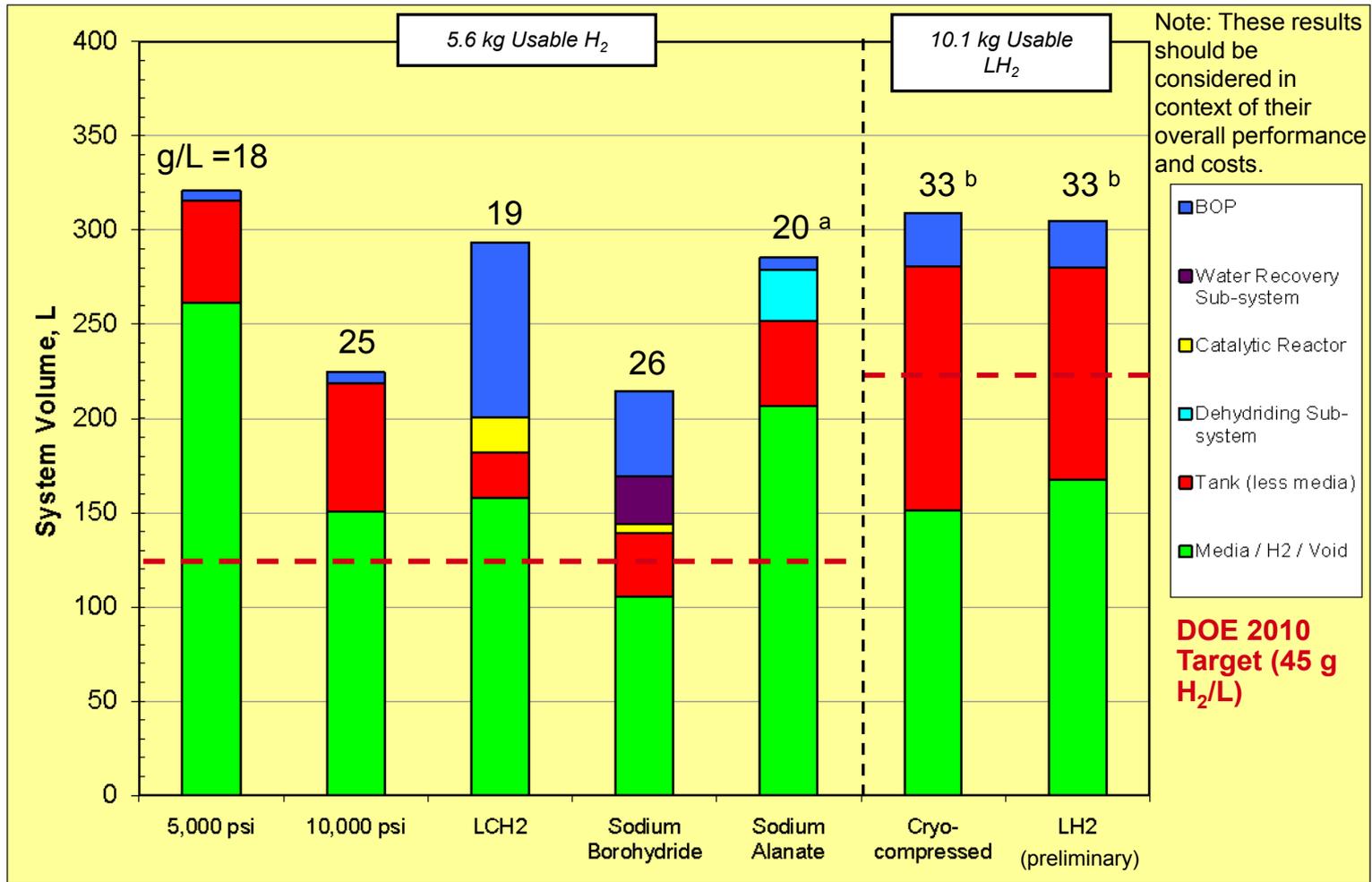
The 5,000-psi tank system may just meet the DOE 2010 gravimetric target of 6 wt%, but the 10,000-psi tank system is about 20% lower than the 2010 target.



<sup>a</sup> The sodium alanate system requires high temp. waste heat for hydrogen desorption, otherwise the usable hydrogen capacity would be reduced.

<sup>b</sup> Normalizing the cryo-compressed and liquid H<sub>2</sub> systems for 5.6 kg of usable H<sub>2</sub> results in gravimetric capacities of ~4.0 wt% and ~4.4 wt%, respectively.

The volumetric capacities of both compressed tank systems are 40-60% lower than the DOE 2010 target of 45 g H<sub>2</sub>/liter.



<sup>a</sup> The sodium alanate system requires high temp. waste heat for hydrogen desorption, otherwise the usable hydrogen capacity would be reduced.

<sup>b</sup> Normalizing the cryo-compressed and liquid H<sub>2</sub> systems for 5.6 kg of usable hydrogen results in volumetric capacities of ~28 g H<sub>2</sub>/L system volume each.

**“Ownership cost” provides a useful comparison metric that includes both on-board and off-board (i.e., refueling) costs on equal footing.**

Fuel System Ownership Cost Assumptions	Gasoline ICEV	cH <sub>2</sub> FCV <sup>1</sup>	LCH <sub>2</sub> FCV	SBH FCV	LH <sub>2</sub> FCV	Basis/Comment
Annual Discount Factor on Capital	15%	15%	15%	15%	15%	Input assumption
Manufacturer + Dealer Markup	1.74	1.74	1.74	1.74	1.74	Assumed mark-up from factory cost estimates <sup>2</sup>
Annual Mileage (mi/yr)	12,427	12,427	12,427	12,427	12,427	Car vehicle miles traveled divided by total registrations for 2006 <sup>3</sup>
Vehicle Energy Efficiency Ratio	1.0	2.0	2.0	2.0	2.0	Based on ANL drive-cycle modeling
Fuel Economy (mpgge)	31	62	62	62	62	ICEV: Car combined CAFE sales weighted FE estimate for MY 2007 <sup>3</sup>
H <sub>2</sub> Storage Requirement (kg H <sub>2</sub> )	NA	5.6	5.6	5.6	5.6	Design assumption based on ANL drive-cycle modeling
Fuel Price (\$/eq. gal)	3.00	4.32	4.74	10.14	4.74	FCVs: Equivalent H <sub>2</sub> price from Off-board Assessment Base Cases
H <sub>2</sub> Storage System Factory Cost (\$/kWh)	NA	15.6	15.4	5.0	14.00 (prelim.)	H <sub>2</sub> storage cost from On-board Cost Assessment of 5.6 kg usable H <sub>2</sub>

<sup>1</sup> cH<sub>2</sub> FCV option assumes pipeline delivery with 6,250 psi dispensing and 5,000-psi on-board storage system.

<sup>2</sup> Source: DOE, "Effects of a Transition to a Hydrogen Economy on Employment in the United States", Report to Congress, July 2008

<sup>3</sup> Source: U.S. Department of Transportation, NHTSA, "Summary of Fuel Economy Performance," Washington, DC, March 2007

**The implicit assumption in this ownership cost assessment is that each fuel system and vehicle perform equally well and have the same operating lifetime.**

